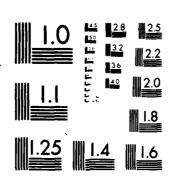
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MX SITING INVESTIGATION GEOTECHNICAL SUMMARY

PRIME CHARACTERIZATION SITES
RIO GRANDE/HIGHLANDS
CANDIDATE SITING PROVINCE

PREPARED FOR

SPACE AND MISSILE SYSTEMS ORGANIZATION (SAMSO)

NORTON AIR FORCE BASE, CALIFORNIA



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MX SITING INVESTIGATION
GEOTECHNICAL SUMMARY
PRIME CHARACTERIZATION SITES
RIO GRANDE/HIGHLANDS
CANDIDATE SITING PROVINCES

Prepared for:

U. S. Department of the Air Force Space and Missile Systems Organization (SAMSO) Norton Air Force Base, California 92409

Prepared by:

Fugro National, Inc. 3777 Long Beach Boulevard Long Beach, California 90807

29 September 1978 15 February 1979 (rev.)

PRIME CHARACTERIZATION SITES RIO GRANDE/HIGHLANDS CSPs

ERRATA

- Replace the following figures with revised ones which accompany this sheet: Figures 6 (p. 16), 7 (p. 18), 13 (p. 38), and 14 (p. 40).
- Replace the following tables with revised ones which accompany this sheet: Tables 5 (p.19 and 20), 14 (p. 41), and 15 (p. 42).

The following corrections are to be made to the original text:

- page 2, Figure 2: Generalized geologic map base revised, see Figure 6.
- page 7, Section 2.2, line 3: Change "The..., intermediate..." to read "Fluvial deposits cover approximately six percent of the area, younger alluvial fan deposits cover approximately 14 percent, intermediate..."
- page 25, first 3 lines: Delete first three printed lines, duplication from page 23.
- page 33, Figure 10: Generalized geologic map base revised, see Figure 13.

FOREWORD

This report was prepared for the Department of the Air Force, Space and Missile Systems Organization (SAMSO) in compliance with conditions of Contract No. F04704-77-C-0010, and is a geotechnical summary of the prime Characterization sites in the Rio Grande and Highlands Candidate Siting Provinces (CSPs). The prime site in the Rio Grande CSP is Jornada del Muerto, New Mexico and the prime site in the Highlands CSP is San Simon Valley, Arizona.

The report presents representative data obtained from geotechnical field investigations performed at both sites as part of the Characterization program. The information obtained from these studies, in combination with data obtained in the Screening studies, has been used for geotechnical ranking (FN-TR-25).

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1.0 INTRODUCTION

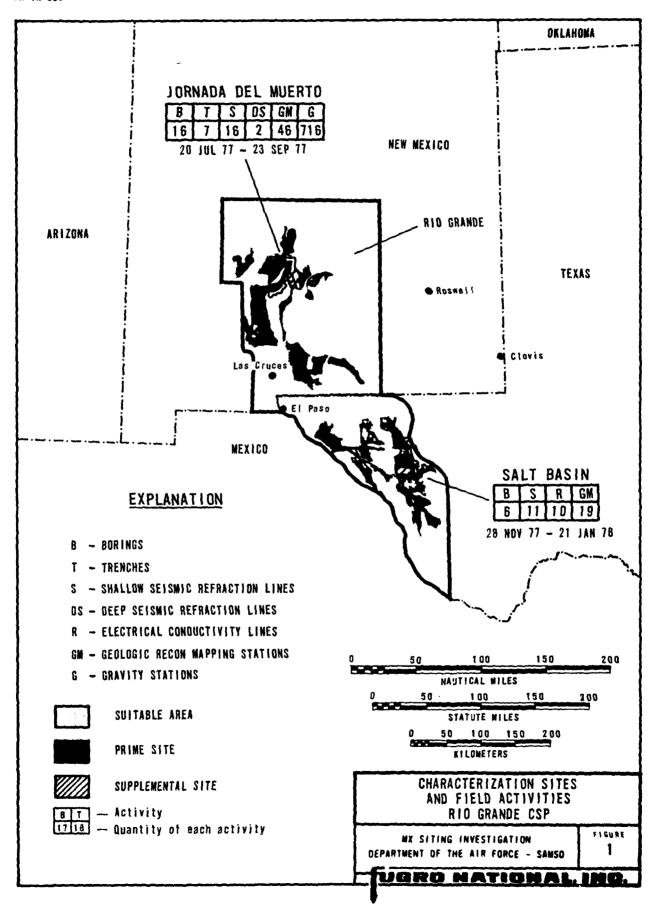
This report presents the results of geotechnical field investigations performed in the Jornada del Muerto and San Simon characterization sites, located in central New Mexico in the Rio Grande Candidate Siting Province (CSP) and in southeastern Arizona in the Highlands CSP, respectively. These provinces are two of six selected for geotechnical characterization studies. This report presents representative data collected and analyzed for these sites. Access to the remaining data can be arranged through SAMSO/MNND, Norton Air Force Base, California.

The Rio Grande CSP lies within the states of New Mexico and Texas (Figure 1). It is characterized by predominately north and northwest trending mountain ranges separated by fault controlled closed basins possessing a variety of geologic and engineering conditions.

The Highlands CSP lies within the states of New Mexico and Arizona (Figure 2) and is characterized by variable geologic structures and topography. North to northwest trending mountain ranges comprise from 25 to 33 percent of its area. Drainage is moderately well developed, however, a few basins are closed and contain playas.

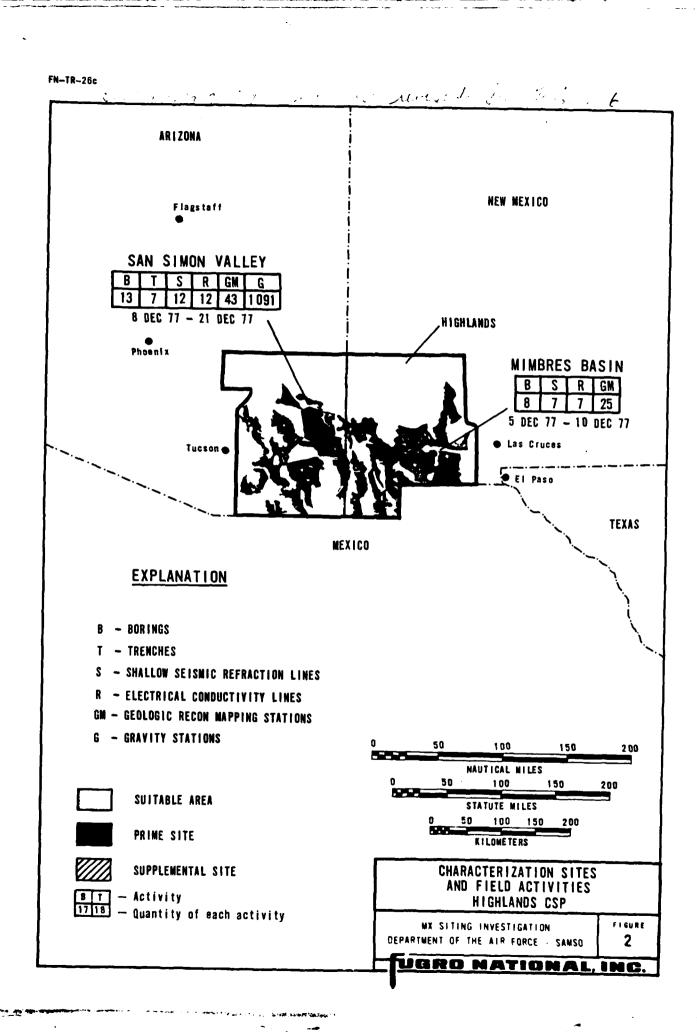
Suitable areas for deployment of MX missile system remaining after Intermediate Screening were divided into CSPs based on similar geotechnical characteristics. The results of Intermediate Screening (FN-TR-17) indicated that existing data

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were not adequate in type or level of detail for follow-on geotechnical and geo-environmental evaluations, screening, site selection, and ranking studies. Therefore, the Characterization studies were developed to provide a rapid, relatively inexpensive method of gathering geotechnical data in small areas (maximum about 700 nm²; 2400 km²) which are considered to be representative of a larger area within the CSP.

Emphasis was placed on the collection of information allowing characterization of geological units with respect to the construction aspects of MX missile basing options. Objectives of the Characterization studies were to obtain data that address the following geotechnical aspects:

- o Surficial geology and terrain
- o Subsurface conditions
- o Geophysical properties
- o Engineering properties

Although the program originally emphasized data collection for the trench and horizontal shelter basing modes, the data were utilized for evaluation of the vertical shelter basing mode as well. Characterization was, therefore, a refinement of the screening process whereby the necessary geotechnical information was developed to support the broader MX system design activities. These activities were taking place concurrently and provided a more firm basis from which to geotechnically rank the remaining suitable area considering different alternative basing modes.

Two Characterization sites (one prime and one supplementary) were selected within each CSP (Figures 1 and 2). This report discusses only the prime site within each CSP.

The characterization site selection process began with a delineation of geotechnically similar areas within each CSP having analogous depositional and geologic histories, rock and water depths, and tectonic settings. Once these areas had been identified, non-geotechnical factors were applied to delineate the actual Characterization site boundaries. These non-geotechnical selection factors included access, proximity to support facilities, environmental sensitivities, and local logistical requirements.

Geologic, geophysical, and soils engineering techniques were used to determine the surface and subsurface geotechnical conditions in Jornada del Muerto and San Simon. These include:

- o Analysis of available data
- o Aerial photo interpretation of surficial geologic units utilizing black and white stereographic pairs at scales of approximately 1:30,000 (Jornada del Muerto) and 1:60,000 (San Simon)
- o Geologic field check of aerial photo interpretation and determination of physical properties of the surficial units at selected field stations
- o Shallow and deep seismic refraction, down hole seismic velocity, and electrical conductivity surveys to obtain subsurface profile information

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- o Gravity and ground magnetic surveys to aid in interpretation of basin configuration
- o Drilling and trenching to determine subsurface soil characteristics and obtain soil samples
- o Laboratory testing of soil samples to determine engineering properties

Prior to initiating any field work, an archeological and environmental inspection was conducted at each site to ensure minimal impact to the local environment and to avoid damage to archeologic and historic sites. To further minimize potential impacts, all field activities were performed adjacent to existing roads or other previously disturbed areas.

Site access to the Jornada del Muerto and Salt Basin characterization sites in the Rio Grande CSP was coordinated through the Base Engineers Office, White Sands Missile Range, and the U.S. Army Corps of Engineers, respectively. Access to characterization sites in the Highlands CSP was gained through BLM permits and the U.S. Army Corps of Engineers.

2.0 JORNADA DEL MUERTO SITE

The Jornada del Muerto characterization site covers an area of 330 nm² (1132 km²) in Socorro and Sierra counties, New Mexico. The site is bounded by mountain ranges on the east and south. The Rio Grande River lies just outside the site area to the west. Chupadera Mesa lies to the north. A network of paved and graded roads as well as four-wheel drive trails provide access within the site.

2.1 SCOPE OF INVESTIGATION

Scope of geologic, geophysical, and soils engineering field activities performed at the site and laboratory tests performed on soil samples from the site is presented in Table 1. Detailed information about the soils engineering field activities (17 borings and seven trenches) is summarized in Tables 2 and 3. Locations of all the field activities are shown in Figure 3.

2.2 SURFICIAL GEOLOGY AND TERRAIN

Alluvial fan deposits of younger and intermediate age and eolian sheet sand are the predominant surficial geologic units within the Characterization site (Figure 3). Fluvial deposits cover approximately 6 percent of the area, younger alluvial fan deposits cover approximately 14 percent, intermediate alluvial fan deposits cover 22 percent, and eolian sheet sand covers approximately 45 percent. Playa and older lacustrine deposits cover approximately three and nine percent of the surface area, respectively. These deposits do not represent a large percentage of the surface area, but they are generally of great thickness and interfinger with alluvial

GEOLOGY AND GEOPHYSICS

TYPE OF ACTIVITY	NUMBER OF ACTIVITIES
Geological mapping stations	46
Shallow refraction	16
Deep refraction	2
Downhole velocity	3
Gravity survey	7 16

ENGINEERING

NUMBER OF BORINGS	NOMINAL DEPTH FEET (METERS)	
13	100 (30)	
3	300 (91)	
		
NUMBER OF TRENCHES	NOMINAL DEPTH FEET (METERS)	
1	16 (5)	
6	18 (6)	

ENGINEERING-LABORATORY TESTS

TYPE OF TEST	NUMBER OF TESTS
Moisture/density	237
Specific gravity	19
Sieve analysis	130
Hydrometer	53
Atterberg limits	90
Consolidation	10

TYPE OF TEST	NUMBER OF TESTS
Unconfined compression	29
Triaxial compression	15
Direct shear	30
Compaction	7
CBR	3
Chemical analysis	8

SCOPE OF FIELD AND LABORATORY ACTIVITIES JORNADA DEL MUERTO, NEW MEXICO, RIO GRANDE CSP

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TABLE 1

BORING NUMBER	TOTAL DEPTH FEET (METERS)	TYPE OF DRILL RIG USED	TYPE OF SAMPLES* OBTAINED
JM-8-1	102.0 (31.1)	Rotary Wash	B, P
JM-B-2	108.0 (32.9)	Rotary Wash	B, P, C
JM-8-3	105.0 (32.0)	Rotary Wash	B, P
JM-B-4	102.5 (31.2)	Rotary Wash	Р
JM-B-5	100.0 (30.5)	Rotary Wash	B, P
3M-B-6	101.0 (30.8)	Rotary Wash	B, P
JM-8-7	102.5 (31.2)	Rotary Wash	P, D, C
JM-B-8	99.0 (30.2)	Rotary Wash	B, P
JM-8-9	102.5 (31.2)	Rotary Wash	8, P, SS
JM-B-10	301.5 (91.9)	Rotary Wash	B, P
JM-B-11	304.0 (92.7)	Rotary Wash	В, Р
JM-B-12	102.5 (31.2)	Rotary Wash	B, P
JM-B-13	101.0 (30.8)	Rotary Wash	8, P
JM-B-14	102.5 (31.2)	Rotary Wash	B, P
JM-B-15	302.5 (92.2)	Rotary Wash	B, P
JM-B-17	102.0 (31.1)	Rotary Wash	B, P, SS
	·		
		i	I

*P = Pitcher sample (undisturbed)

D = Fugro Drive sample (relatively undisturbed)

B = Bulk sample (disturbed, but representative)

SS = Split Spoon sample (disturbed, but representative)

C = Rock Core

ENGINEERING	FIELD ACTIVITIES - BORINGS
JORNADA	DEL MUERTO, NEW MEXICO
	RIO GRANDE CSP

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DEPARTMENT OF THE AIR FORCE SAMSO

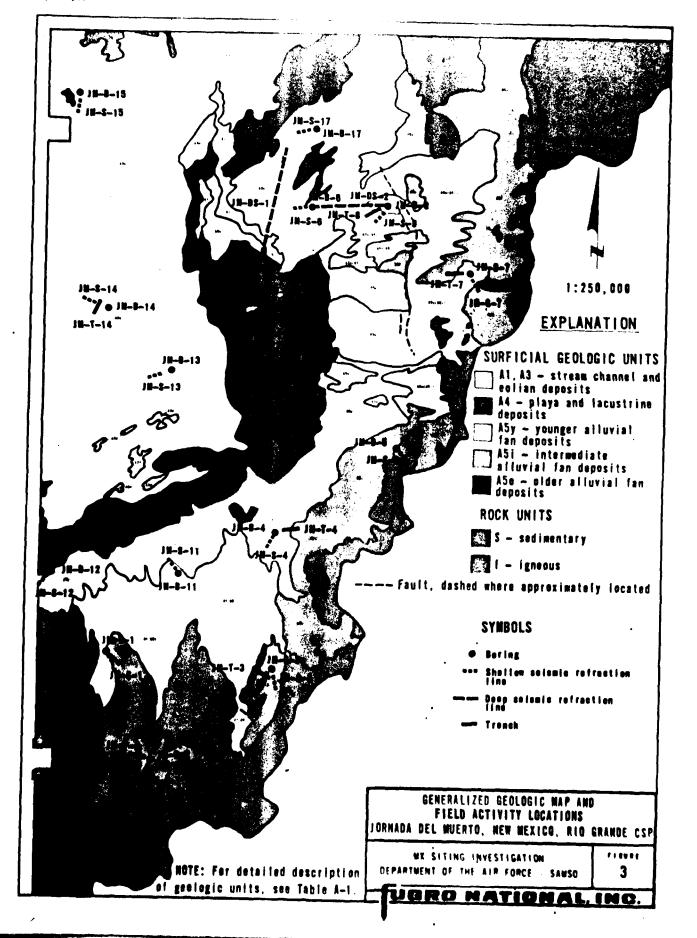
TABLE 2

TRENCH NUMBER	TOTAL DEPTH FEET(METERS)	STABILITY OF VERTICAL EXCAVATION WALLS
JM-T-2	16.5 (5.0)	stable; 15.5-16.5° (4.7-5.0m), stage Ⅲ Caliche
JM-T-3	18.0 (5.5)	stable; 16.5-18.0° (5.0-5.5m), stage II Caliche
JM-T-4	18.0 (5.5)	stable
JM-T-7	18.0 (5.5)	stable; 1-3' (0.3-0.9m) , stage I Caliche
JM-T-8	18.0 (5.5)	stable; 0-7' (0-2m) some sloughing into trench; 7-17' (2.1-5.2m) stable; 17-18' (5.2-5.5m) stage I Caliche, 3-9' (0.9-2.7m)
JM-T-12	18.0 (5.5)	stable; 3-12° (0.9-3.7m), stage I Caliche
JM-T-14	18.5 (5.6)	unstable; heavy sloughing, 0-5' (0-1.5m) stable; stage I Caliche, 5-10' (1.5-3.0m) unstable; some sloughing into trench, 10-18.5' (3.0-5.6m)

ENGINEERING FIELD ACTIVITIES - TRENCHES
JORNADA DEL MUERTO, NEW MEXICO
RIO GRANDE CSP

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO

TABLE



deposits in the subsurface within the construction zone. The alluvial fan deposits are typically silty sands with gravel, ranging from sandy gravels near the mountain fronts to sandy silts near the playas. Playa and older lacustrine deposits are generally clayey silts. These units along with the remaining surficial units are described in Table 4.

Surface slopes and depths of drainage incision vary with geologic units, both generally increasing with proximity to the mountain fronts (Table 4). Maximum surface slope is five percent with typical slopes of less than one percent. Drainages are typically shallow (less than 10 feet; 3 m), with gently sloping sides except near mountainous areas. Locally they may be deep (greater than 20 ft; 6 m) and steep sided.

2.3 SUBSURFACE CONDITIONS

2.3.1 Soil Profiles

Varying thicknesses of eolian sheet sand and alluvial fan deposits typically overlie several hundred feet of older lacustrine deposits in the Jornada site. The subsurface conditions and the composition of the soils with depth are illustrated by the soil profiles shown in Figures 4 and 5. Eolian sheet sand and alluvial deposits predominantly consist of coarse-grained soils whereas lacustrine deposits consist of fine-grained soils.

2.3.2 Depth to Shallow (<150 ft;<46 m) Rock and Water

Figure 6 shows the portions of the site in which rock and water

are estimated to be encountered within a depth of 150 feet

		THICKNESS		USCS	AREAL EXTE	NT (SITE)
SURFICIAL GEOLOGIC UNIT (a)	GEOLOGIC AGE	FEET (METERS)	DESCRIPTIVE NAME(S)	(p)	nm ² (km ²)	PERCENT
Fluvial Deposits (A1)	Quaternary	Unknown	Silty Sand with Clay	SM	20 (69)	6
Eolian Deposits Sheet and Dune Sand (A3s, A3d)	Quaternary	0-18	Sand, Silty Sand, Silty Sand with Clay	SP, SM	149 (511)	45
Playa Deposits (A4)	Quaternary	Unknown	Silt and Clay	ML, CL	10 (34)	3
Older Lacustrine and Playa Deposits (A4o)	Quaternary- Tertiary	Unknown	Clay, Gypsiferous Silt. Silty Sand	CL. ML. SM	30 (103),	9
Younger Alluvial Fan Deposits (A5y)	Quaternary	Unknown	Silty and Clayey Sand with Gravel, Silt, Clay	SM, SC	46 (158)	14
Intermediate Alluvial Fan Deposits (A5i)	Quaternary	Unknown	Silty Sand with Gravel and Cobbles	SM	73 (250)	22
Older Alluvial Fan Deposits (A5o)	Quaternary- Tertiary	Unknown	Sandy Gravel with Cobbles and Boulders	SP-GW	3 (10)	1
						. 1

NOTES

- (a) For generic description of geologic units, see Table A-1.
- (b) For description of USCS, see Table A-2.
- (c) For description of stage of caliche, see Figure A-1.
- (d) Mixed with A5i deposits in the southerm part of the site; designated A1 A5y on Figures 3 and 6
- (e) Dune sands comprise one percent of the site area.
- (f) This gypsiferous deposit occurs extensively in the subsurface.

REAL EXT	NT (SITE)	<u> </u>	PROPERTIE	S OF SURFACE	MATERIALS	<u> </u>	SURFACE I	MORPHOLOGY	
n ² (km ²)	PERCENT	GRADATION	CEMENTATION	MAXIMUM GRAIN SIZE	PAVEMENT/ PATINA	STAGE OF Caliche (c)	SLOPE (PERCENT)	DRAINAGE DEPTHS FEET(METERS)	NOTES
(69)	6	Well	None- Moderate	Sand	None/None	I	<	None	(d)
19 (511)	45	Poor- Moderately well	None- Weak	Sand	None/None	I	< 1	<1	(e)
0 (34)	3	Poor	None- Weak	Silt	None/None	None	< 1	None	
0 (103),	9	Poor	Weak-Strong	Sand	None/None	None-Ⅲ	< 1	0-5 (0-2)	(1)
6 (158)	14	Moderately well	None-Weak	Sand	None/None	I	1-4	<1-6 (<1-2)	
3 (250)	22	Moderately well-Well	Moderate- Strong	Cobble	Poor/Poor	п	2-9	5-25 (2-8)	
3 (10)	1	Moderately well	Moderate- Strong	Boulder	None /None	п-ш	9-12	50-100 (16-33)	
									

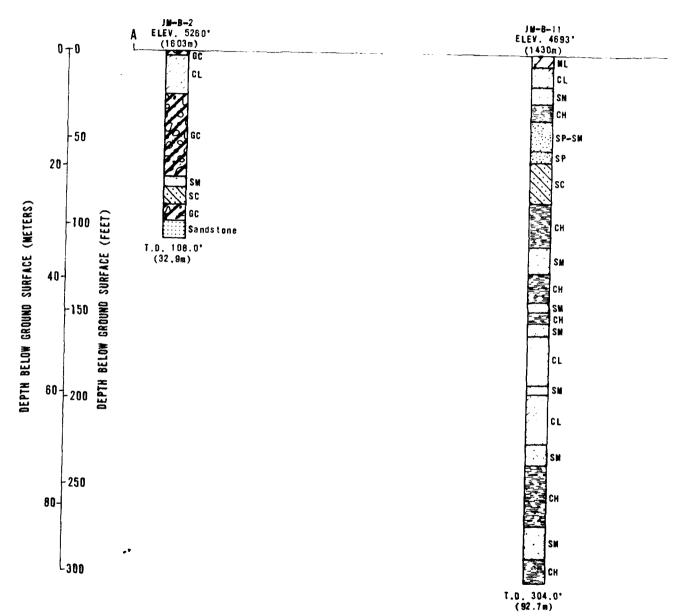
DESCRIPTION OF SURFICIAL GEOLOGIC UNITS

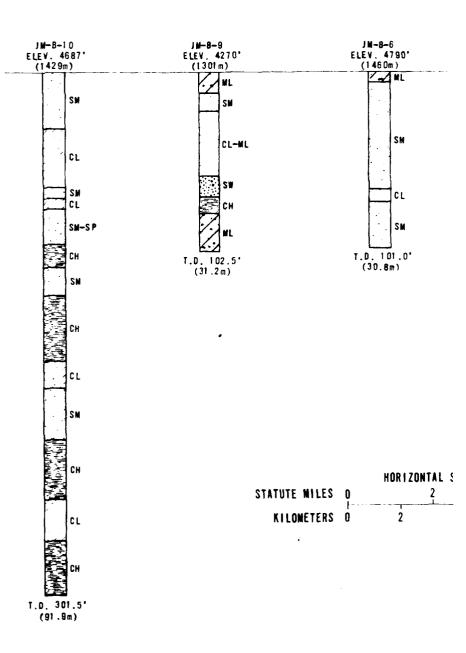
JORNADA DEL MUERTO, NEW MEXICO, RIO GRANDE CSP

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TABLE 4

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NOTES: 1. Ground surface elevations shown at locations of bori

2. T.D.=Total Depth

 Soil types shown adjacent to soil column are based ((USCS) and are explained in the appendix

J

300-

LOCATION MAP

A'

JIM-B-17

JIM-B-6

JIM-B-10

SCALE

ings are approximate

on Unified Soil Classification System

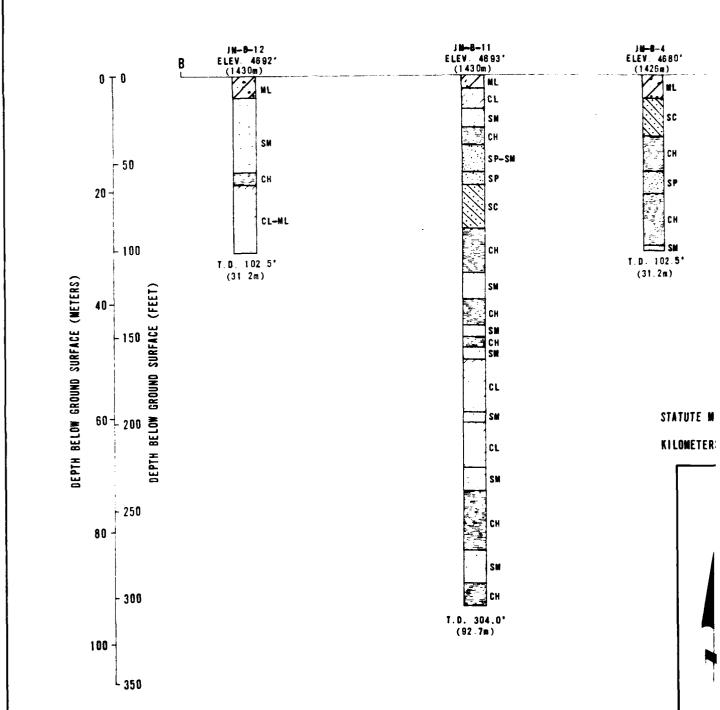
SOIL PROFILE AA'
JORNADA DEL MUERTO, NEW MEXICO
RIO GRANDE CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SAN

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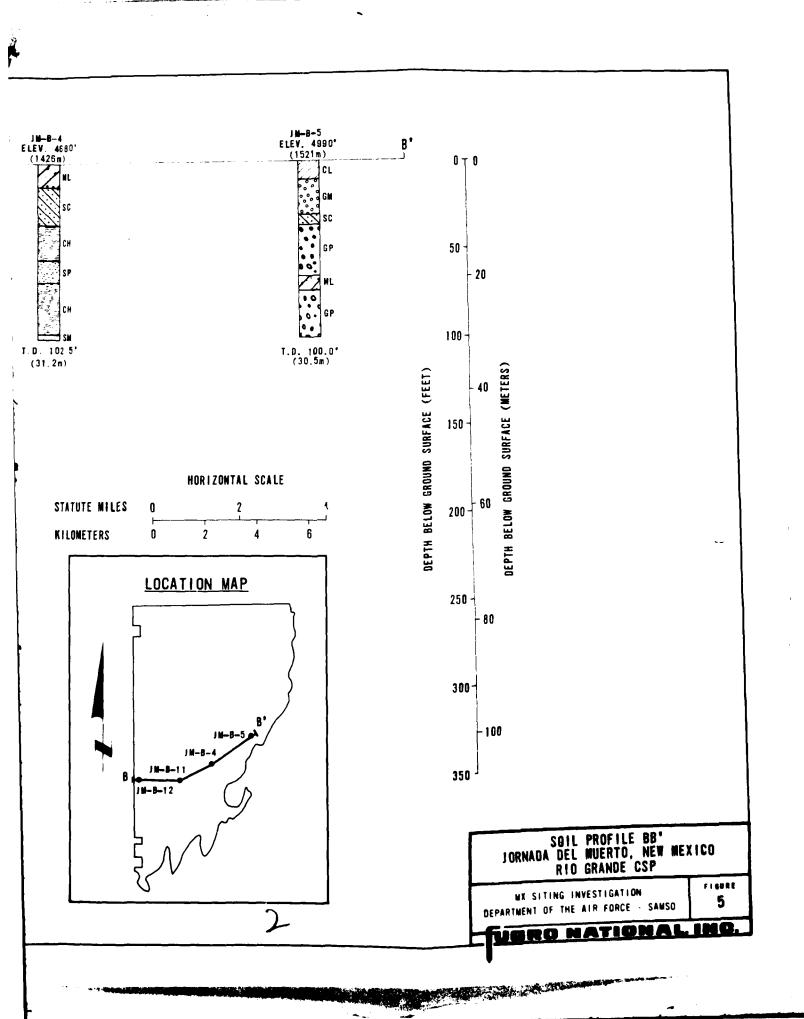
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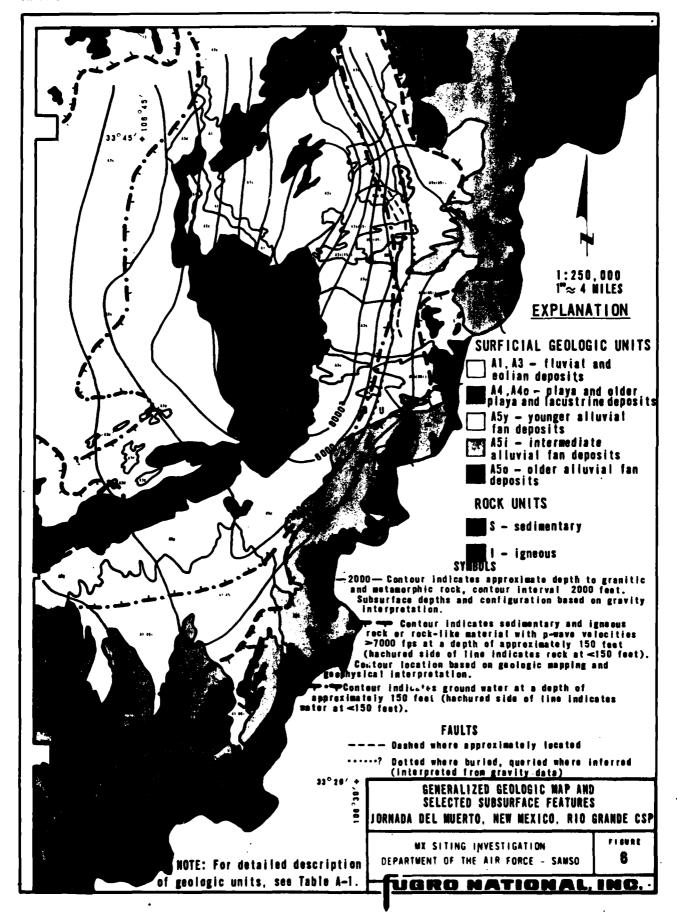
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NOTES: 1. Ground surface elevations shown at locations of borings are approximate

- 2. T.D.= Total Depth
- 3. Soil types shown adjacent to soil column are based on Unified Soil Classification System (USCS) and are explained in the appendix





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below ground surface. Shallow rock comprises approximately ten percent of the site based on boring, seismic, gravity, geologic, topographic and other available data. Ground water will be encountered at depths of less than 150 feet (46 m) over approximately 30 percent of the site area. Areas of shallow ground water will generally coincide with the surficial distribution of older lacustine and playa deposits. Elsewhere, local areas of perched water may also be encountered at depths of less than 150 feet (46 m).

2.3.3 Basin Configuration

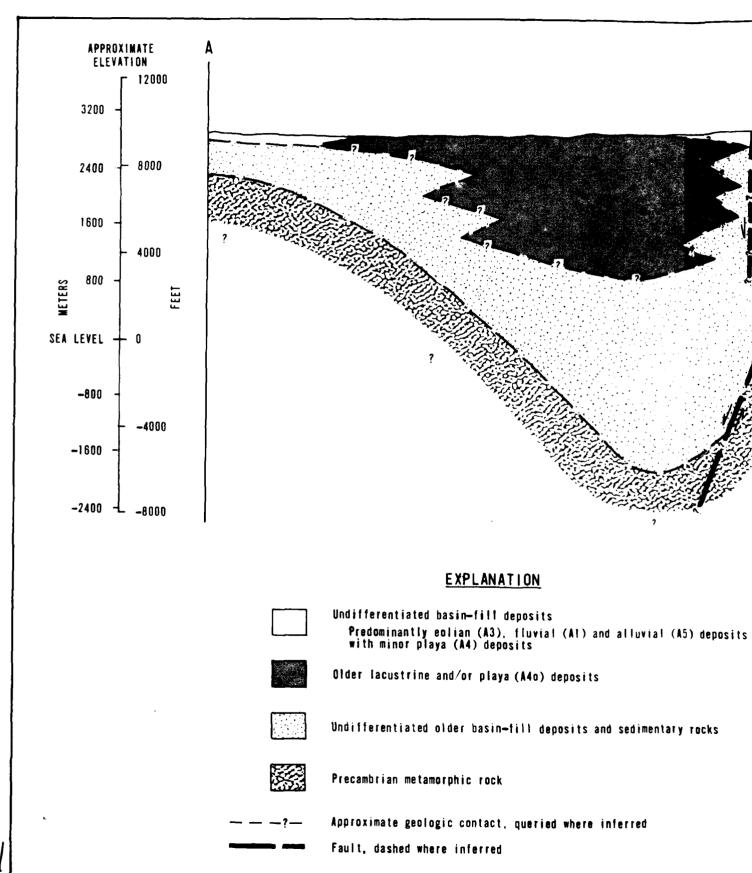
Geophysical investigations indicate bedrock within 50 feet (15 m) of the surface near the mountains in the southern part of the site. Deep seismic lines near the middle of the valley encountered high velocity materials, probably well indurated older alluvium, at a depth of 450 feet (140 m).

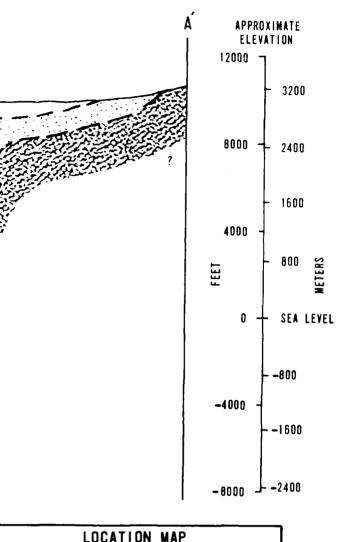
Gravity data indicate the basement topography of the site is dominated by a 16,000-foot (4900 m) deep basin that is bounded on the east by a steep fault and on the west by a gently sloping plane in the vicinity of the generalized geologic cross-section (Figure 7). Near the south end of the site, an east-west trending basement ridge separates the large basin from a smaller one. Buried basalt from the Jornada Malpais basalt field may overlie much of this ridge.

2.4 GEOPHYSICAL PROPERTIES

Results of shallow and deep seismic refraction surveys and downhole velocity surveys are presented in Tables, 5, 6 and 7.

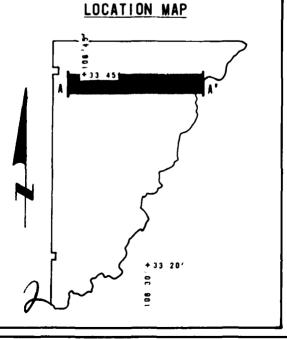






NOTES:

- 1. The cross section is generally representative of subsurface conditions within the band shown on the location map. Due to the limited density of available data and the sparseness of newly acquired data, the subsurface conditions are highly interpretive.
- 2. For a detailed description of geologic units see Table A-1.



Horizontal Scale: 1™ ~ 2 Miles (3km) Vertical Scale: 1™ ~ 4000° (1219m) Vertical Exaggeration: 2.6 X

HORIZONTAL SCALE



GENERALIZED GEOLOGIC CROSS SECTION JORNADA DEL MUERTO, NEW MEXICO RIO GRANDE CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SAMSO

FIGURE 7

SEISMIC LINE NO	NO.				VELO	CITY D	VELOCITY DISTRIBUTION FPS (MPS)	IT I ON F	JW) Sd:	S)		ı		.,l	DEEPER Refractors Depth	*ROCK EXCLUSION DEPTH TO 7000 FPS
1=S-1	S-1 1700 (518)	T G			l l		4800 ((1463)						1	340 (104) 8300 (2530)	(2134 MPS
=) M-S-2 - 1700 ((518)	+				7500 (2286)	2286)				10600	00 (3231)	A	1	
=	1#-S-3 ★ 1850 (5	(264)	4	4450 (1356)	X		720	7200 (2195)						Å		
=	JM-S-4 (518) ►		ļ-				6050 (1844)	1844)						Å		133 (41)
JM-S-5	S-5 1700 (518)	Y					2600 (792)	792)						A		272 (83)
JM-S-6	S-6 1740 (530)	▼					3460 (1055)	1055)						A		264 (80)
JM-S-7		Y					3100 (945)	945)						A		246 (75)
J#-S-8	\vdash						2800 (6	(853)			!	:		A		261 (80)
JM-S-9	S-9 1200 -S			•			3750 (1143)	1143)						Å		243 (74)
	IM-S-10 1560 (475)	(13	372)				7200 (2195)	2195)						À		
	IN-S-11 ← 1700 (518)	A	3800	800 (1158)			6450 (1966)	1986)						À		215 (66)
JIM-S-12	-12						4750 (1448)	1448)			l			Å		246 (75)
`_	IM-S-13 1200 (366)	¥					7000 (2134)	2134)						Å		
	JM-S-14 - 1500 (457)	57)	_	1			3300 (1006)	1006)						Å		313 (95)
				i :											FT (M) FPS (MPS)	FEET (M)
METERS	RS 0	2-		2-	15		20	25		30	35		40	45		
E E	- w - O	<u>-</u>	50	30 4	40 50		60 70 80 Depth interval	80 ERVAL	- 06	- 00	110 120		130 140	0 150		
ULTS	# If no refracting	efracting		interface or layer with denth calculation was ne	layer w	ith a v	h a velocity	greate	greater than 7000 fps	7000 f	ps (rock	/rock-1	(rock/rock-like material)	erial) 1	a velocity greater than 7000 fps (rock/rock-like material) was detected,	±.

TABLE

5

MX SITING INVESTIGATION

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DEEPER * ROCK REFRACTORS EXCLUSION DEPTH TO DEPTH TO TOOO FPS VELOCITY (2134 MPS)	- 251 (76)	- 240 (73)									FPS (MPS) FEET (M)			as detected,
VELOCITY DISTRIBUTION FPS (MPS)	3050 (830)	3900 (1189)										. 10 15 20 25 30 35 40 45	1 60 70 80 90 100	Interface or layer with depth calculation was p
SEISMIC Line no.	J#-S-15 (488) ►	JM-S-17 ~										METERS 0 5	FEET 0 5 10 7	• If no refracting a rock exclusion
							ORN	ADA	DEL R10	MUE	EFRA RTO, NDE	CTII NEV CSP	ON RE	SULTS (100

VELOCITY LAYER	COMPRESSIONAL WAVE VELOCITY FPS (MPS)	AVERAGE THICKNESS FT (M)	COMMENTS
1	2000 (610)	20 (6)	
2	4000 (1219)	150 (46)	
3	6200 (1890)	300 (91)	Begin Saturated Sediments
4	7500 (2286)	700 (213)	
5	9000 (2743)	Undetermined	

DEEP SEISMIC REFRACTION RESULTS JORNADA DEL MUERTO, NEW MEXICO RIO GRANDE CSP

MX SITING INVESTIGATION

TABLE

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6

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WAVE TYPE	d	s		a	S	Q.	S		
						6000 (1829)	1460 (445)	35 40 45	
ION FPS (MPS)	5000 (1524)		6600 (2012)	2725 (830)	4500 (1372)	1200 (366)	90 100		
VELOCITY DISTRIBUTION FPS (MPS)							2120 (646)	1200	15 20 21 50 60 70 80 DEPTH INTERVAL
	(613)	2030 (619)		4150 (1264)	1650 (503)	3080 (838)	10 (561)	20 30 40	
6	2010	1120 (341)		1650 (503)	1000 (305)		184	6-	
DOWNHOLE SURVEY NO.	15			IM-DH-2		J.W_DH-10		METERS FEET	
								DOWNHOLE VELOCITY SURVEY RESULTS JORNADA DEL MUERTO, NEW MEXICO RIO GRANDE CSP	
								MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO 7	

Shallow refraction results (Table 5) indicate a surficial layer having a velocity range between 1200 and 1850 fps (366 and 564 mps) with an average thickness of eight feet (2.5 m). Velocities greater than 7000 fps (2134 mps) were encountered at the location of four lines. Five major velocity zones were observed on the deep seismic lines (Table 6). Velocities representative of crystalline basement were not observed.

The compressional wave velocities from downhole surveys

(Table 7) do not correspond with those from shallow seismic refraction (Table 5) due to the anisotropy of the soils and method of measurement. However, shear wave velocities of the site soils were obtained from the downhole surveys.

2.5 ENGINEERING PROPERTIES

Engineering properties of the subsoils representing various geologic units were determined from laboratory tests. The tests consisted of the following: classification, consolidation, shear strength, compaction, CBR, and chemical. The range of engineering properties and compressional wave velocityes are presented in Table 8.

Eolian sheet sand consists of medium dense to dense poorly graded sands and silty and clayey sands with little gravel. Intermediate alluvial fan deposits consist of dense to very dense sands and gravels. Younger alluvial fan deposits are comprised of medium dense to dense silty and clayey sands with some stiff silts and clays. Older lacustrine deposits consist of stiff to very stiff silts and clays which are

ENGINEERING AND GEOPHYSICAL PROPERTIES	Eolian sheet sand (A3s)	Intermediate
	SP. SM. SC.	Intermediate alluvial fun
UNIFIED SOIL CLASSIFICATION SYMBOL(S) GENERAL PROPERTIES	or, om. ou.	SP. SM, SC, GP. G
DRY DENSITY pcf(kg m ³)	100-120 (1602-1922)	DE 122 / 1520m 25
MOISTURE CONTENT (%)	7-17	95-133 (152 2 -21) 7-19
DEGREE OF SATURATION (3)	30-78	47-83
SPECIFIC GRAVITY	2.64-2.66	2.68-2.77
DEGREE OF CEMENTATION	None to moderate	Moderate to st
COMPRESSIONAL WAVE VELOCITIES fps(mps)	1420-3220 (433-981)	1000-7200 (305-
ELECTRICAL CONDUCTIVITY (mhos m)	DNA	DNA
GRAIN SIZE DISTRIBUTION (2)	<u>=::::::</u>	
BOULDERS >12 inches(30cm)	0-5	0-3
COBBLES 3 to 12 inches(8to 30cm)	0-5	0-10
GRAVEL	0-12	0-90
SAND	50-97	5-95
SILT AND CLAY	3-50	5-48
PLASTICITY DATA		
LIQUID LIMIT	20±	24-26
PLASTICITY INDEX	NP-7	NP-12
COMPRESSIBILITY DATA		
COMPRESSION AT 4 ksf(192kN/m²) (5)	DNA	DNA
SWELL OR COLLAPSE UPON SATURATION (1)	DNA	DNA
SHEAR STRENGTH DATA		
UNCONFINED COMPRESSION ksf(kn m²)	DNA	2.0 ± (96 ±
CD TRIAXIAL COMPRESSION	c = 0-1.0 ksf (48 kN m ²), φ = 34°-39°	DNA
DIRECT SHEAR ks/(kn m²)	0.7-5.5 (34-263)	2 5-7.7 (120-
COMPACTION AND CBR DATA		
MAXIMUM DRY DENSITY pcf(kg m ³)	125-138 (2002-2211)	DNA
OPTIMUM MOISTURE CONTENT (%)	6.0-8.5	DNA
CBR AT 90% RELATIVE COMPACTION	16±	DNA

DNA - DATA NOT AVAILABLE (INSUFFICIENT DATA OR TESTS NOT PERFORMED)

GEOLOGI	C UNITS	
ediate alluvial fun deposits (A5i)	Younger alluvial fan deposits (A5y)	Older lacustrine deposits (A4o)
SP. SM, SC, GP. GM. GC	SM. SC. ML. CL	CL. ML. SC
95-133 (1522-2130)	80-116 (1281-1858)	84-120(1346-1922)
7-19	4-20	3-43
4,-83	19-49	10-89
2.68-2.77	2 67-2 72	2.59-2.73
Moderate to strong	None to weak	Weak to strong
1000-7200 (305-2195)	1500-3100 (457-945)	1700-6750 (518-2057)
DNA	DNA	DNA
0-3	0-3	0
0-10	0-10	0
0-90	0-20	0-15
5-95	7-75	5-95
5 - 48	10-85	5-95
24-26	24-27	21-66
NP-12	NP-13	NP-31
DNA	DNA	1 5-4 5
DNA	DNA	0 1-3 O(Swell)
2.0±(96±)	0.75 ± (36 ±)	0.5-8.2 (24-393)
DNA	DNA	$c = 0 - 1.5 \text{ ksf} (72 \text{ kN m}^2), \phi = 18^{\circ} - 34$
2 5-7.7 (120-369)	DNA	1.7-6.7(81-321)
DNA	136 ± (2179 ±)	121-126 (19 36- 20!8)
DN A	6.0±	9.0-9.5
ON A	18±	7±

RANGE OF ENGINEERING AND GEOPHYSICAL PROPERTIES JORNADA DEL MUERTO. NEW MEXICO, RIO GRANDE CSP

WX SITING INVESTIGATION

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TABLE B

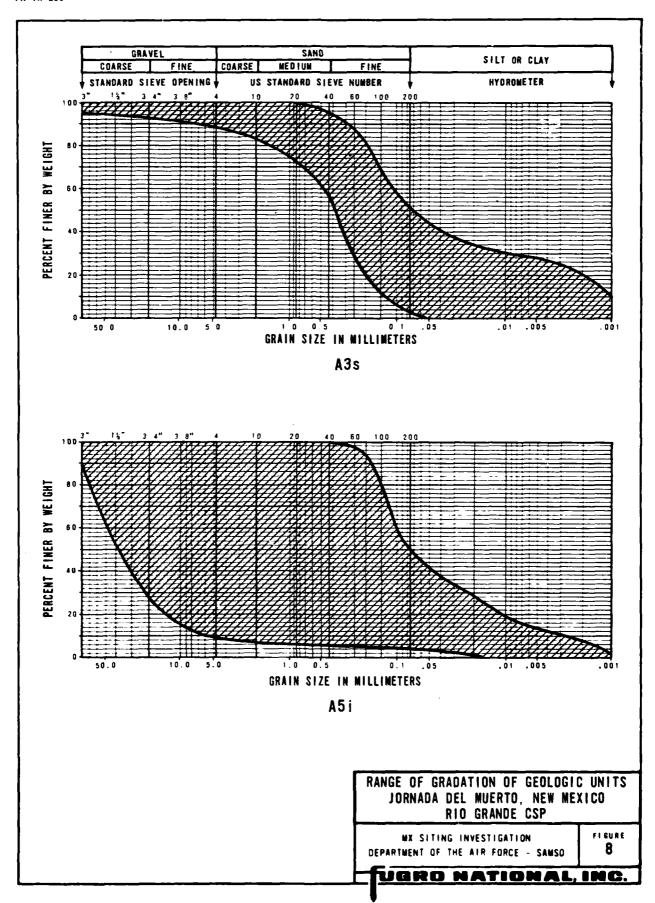
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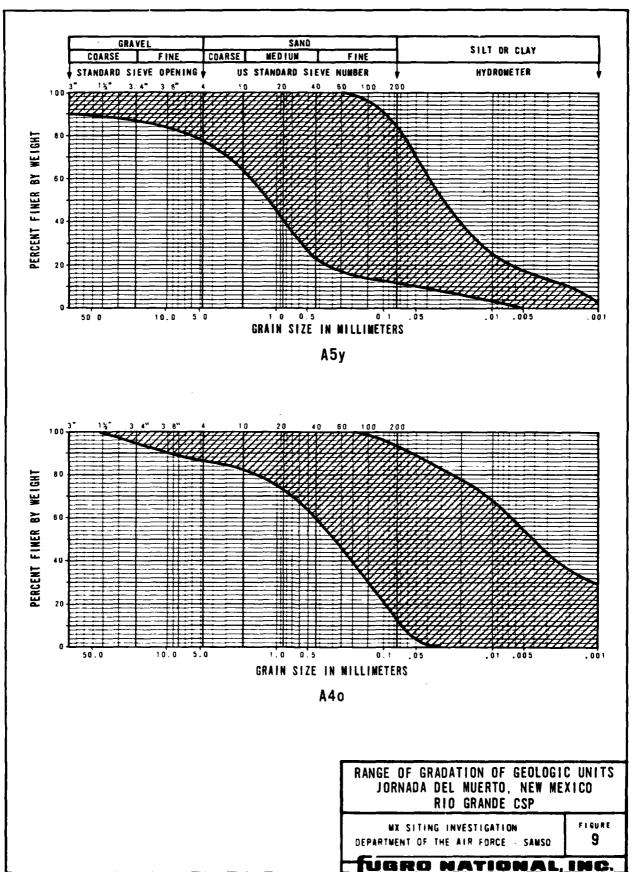
with some stiff silts and clays. Older lacustrine deposits consist of stiff to very stiff silts and clays which are moderately compressible. Eclian sheet sand and intermediate alluvial fan deposits possess moderately high shear strengths; younger alluvial fan and older lacustrine deposits possess moderate shear strengths. The site soils are generally neither expansive nor collapsible. Range of the gradation of the four geologic units is shown in Figures 8 and 9.

Results of chemical tests on soil samples are shown in Table 9.

The test results indicate that sulfate attack of soils on concrete will be "severe."

Representative logs of three borings and three trenches from the site are contained in Appendix B. Results of the shear strength and CBR tests performed on soil samples from the site and a summary of all the laboratory tests performed on soil samples obtained from boring JM-B-ll are also included in Appendix B.





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IRENCH NO.		CAMPIE LETEBOAT				¥	WATER SOLUBLE		CALCIUM
-	SAMILE	3 C 2 C 2 C 2 C 2 C 2 C 2 C 2 C 2 C 2 C	SUIL	푎	MOTOOS	CHLORIDE	SULPHATE	CALCIUM	CARBONATE
Ļ	FEET	METERS	•		mg/kg	mg/kg	mg/kg	mg/kg	mg/kg
4	15.8-17.3	4.82-5.27	70	7.4	345	109	0096	2900	7250
JM-8-9 P-2	10.8-11.8	3.29-3.60	1	7.6	75	33	7940	3150	7875
JM-8-10 P-2	10.0-10.7	3.05-3.26	H	7.4	975	195	10500	3580	8950
JM-B-13 P-2	10.0-11.8	3.05-3.60	ತ	7.4	500	242	11000	3100	7750
JM-8-14 P-1	5.0-7.5	1.52-2.29	35	8.0	185	29	377	11	192
JM-8-17 P-3	10.0-11.1	3.05-3.38	N.	7.5	61	10	0096	2920	7300
JM-T-4 8-2	3.5-6.0	1.07-1.83	¥	7.3	83	38	8340	3220	8050
JM-T-12 8-1	3.0-5.0	0.91-1.52	¥	7.4	116	43	9260	3300	8250

SUMMARY OF CHEMICAL TEST RESULTS JORNADA DEL MUERTO, NEW MEXICO RIO GRANDE CSP

MX SITING INVESTIGATION
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TABLE

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3.0 SAN SIMON SITE

The San Simon characteriztion site covers an area of 715 nm² (2452 km²) in Graham and Cochise counties, Arizona. The site is bounded by mountain ranges on the east and west. The valley extends beyond the bounds of the site to the north and south. Major streams within the site drain toward the Gila River to the north. The site is accessible via Interstate 10 along the southern edge and via state route 666 along the western edge. A network of graded roads and four-wheel drive trails provides access within the site.

3.1 SCOPE OF INVESTIGATION

Scope of geologic, geophysical, and soils engineering field activities performed at the site and laboratory tests performed on soil samples from the site are presented in Table 10.

Detailed information about the soils engineering field activities (13 borings and seven trenches) is summarized in Tables 11 and 12. Locations of all the field activities are shown in Figure 10.

3.2 SURFICIAL GEOLOGY AND TERRAIN

Alluvial fan deposits of younger and intermediate age and older lacustrine deposits are the predominant surficial geologic units within the San Simon site (Figure 10). Younger alluvial fans cover approximately 35 percent of the area, intermediate alluvial fans cover 25 percent, and older lacustrine deposits cover 30 percent. The alluvial fan deposits are typically silty sands with gravel, ranging from sandy gravels near the mountain front to sandy silts near the valley interiors. The lacustrine

GEOLOGY AND GEOPHYSICS

TYPE OF ACTIVITY	NUMBER OF ACTIVITIES
Geological mapping stations	43
Shallow refraction	12
Conductivity	12
	-

ENGINEERING

NUMBER OF BORINGS	NOMINAL DEPTH FEET (METERS)
1	25 (8)
9	50 (15)
2	100 (30)
1	300 (91)
NUMBER OF TRENCHES	NOMINAL DEPTH FEET (METERS)
2	10 (3)
5	12 (4)

ENGINEERING-LABORATORY TESTS

TYPE OF TEST	NUMBER OF TESTS
Moisture/density	135/99
Specific gravity	4
Sieve analysis	66
Hydrometer	50
Atterberg limits	37
Consolidation	4

TYPE OF TEST	NUMBER OF TESTS
Unconfined compression	9
Triaxial compression	4
Direct shear	24
Compaction	6
CBR	2
Chemical analysis	6

SCOPE OF FIELD AND LABORATORY ACTIVITIES SAN SIMON VALLEY, ARIZONA, HIGHLANDS CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SAMSO

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TABLE

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BORING NUMBER	TOTAL DEPTH FEET (METERS)	TYPE OF DRILL RIG USED	TYPE OF SAMPLES* OBTAINED
SS-B-1	302.5 (92.2)	Rotary wash	0, P
SS-B-2	72.5 (22.1)	Rotary wash	D, P
SS-B-3	50.9 (15.5)	Hollow Stem Auger	\$\$, D
\$\$-B-4	51.0 (15.5)	Hollow Stem Auger	D
\$\$-8- 5	55.5 (16.9)	Hollow Stem Auger	D
\$ S-B- 6	51.0 (15.5)	Hollow Stem Auger	D
SS-B-7	45.0 (13.7)	Hollow Stem Auger	D
8-8-22	54.0 (16.5)	Rotary Wash	D
SS-B-9	48.0 (14.6)	Hollow Stem Auger	D
SS-8-10	20.0 (6.1)	Hollow Stem Auger	B, D
SS-B-11	101.5 (30.9)	Rotary Wash	D, P
SS-8-12	61.0 (18.6)	Rotary Wash	В
SS-B-13	50.0 (15.2)	Hollow Stem Auger	0
	-		

^{*} P = Pitcher sample (undisturbed)

ENGINEERING FIELD ACTIVITIES - BORINGS SAN SIMON VALLEY, ARIZONA HIGHLANDS CSP

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TABLE

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D = Fugro Drive sample (relatively undisturbed)

B = Bulk sample (disturbed, but representative)

SS = Split Spoon sample (disturbed, but representative)

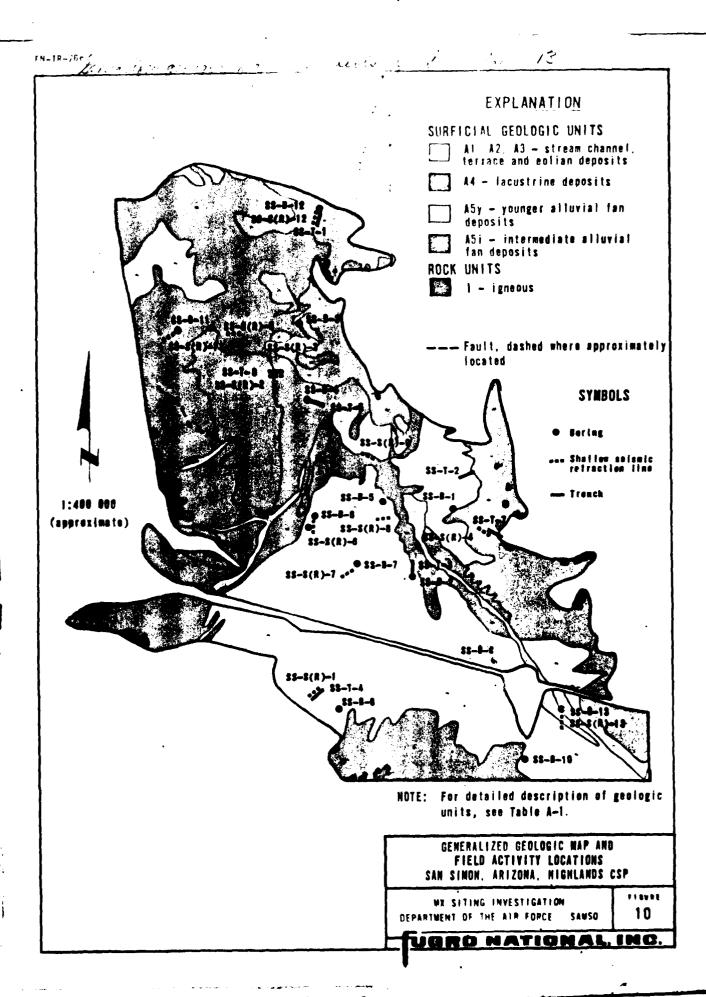
TRENCH NUMBER	TOTAL DEPTH FEET(METERS)	STABILITY OF VERTICAL EXCAVATION WALLS
\$\$-1-1	11.5 (3.5)	stable
SS-T-2	12.5 (3.8)	stable
SS-T-3	12.0 (3.7)	stable
SS-T-4	10.2 (3.1)	stable, some sloughing at 3.5-9.5'(1.1-2.9m)
SS-T-5	12.5 (3.8)	stable
8-1-22	12.8 (3.9)	stable
7-7-22	10.2 (3.1)	stable

ENGINEERING FIELD ACTIVITIES - TRENCHES
SAN SIMON VALLEY, ARIZONA
HIGHLANDS CSP

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO

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JGRO NATIONAL, INC.



deposits are very coarse along the periphery of the valley but are fine grained along the valley axis. These units along with the remaining surficial units are described in Table 13.

Surface slopes and depths of drainage incision vary with geologic units, both generally increasing with proximity to the mountain fronts (Table 13). Maximum observed surface slope was three percent with typical slopes of less than one percent. Drainages are typically shallow (less than 10 ft; 3 m) with gently sloping sides except near mountainous areas and in the older lacustrine material.

3.3 SUBSURFACE CONDITIONS

3.3.1 Soil Profiles

Silty and clayey sands and gravels are the predominant surficial soils which are typically underlain by several hundred feet of clay and silty clay deposits throughout much of the valley. The general subsurface conditions are illustrated by two representative soil profiles shown in Figures 11 and 12. The percentage of fines generally increases towards the valley basin. Cobbles and boulders are encountered only in the close proximity of mountain fronts.

Depth to Shallow (<150 ft; <46 m) Rock and Water

Figure 13 shows portions of the site in which rock and water

are estimated to be encountered within a depth of 150 feet

(46m) below ground surface. Shallow rock exists in approximately five percent of the site based on boring, seismic,

gravity, geologic, topographic, and other available data.

Quaternary	Unknown	Sand and Silt	SM, ML	50 (172)	7
Quaternary- Tertiary	Unknown	Clay, Silt, Sand, Gravel with cobbles and boulders	CL, ML. SP-SW. GP-GW	215 (737)	30
Quaternary	Unknown	Silty sand, Sand with Gravel	SM, SP	243 (833)	35
Quaternary	Unknown	Silty Sand with Gravel	SM	179 (614)	25
	i				

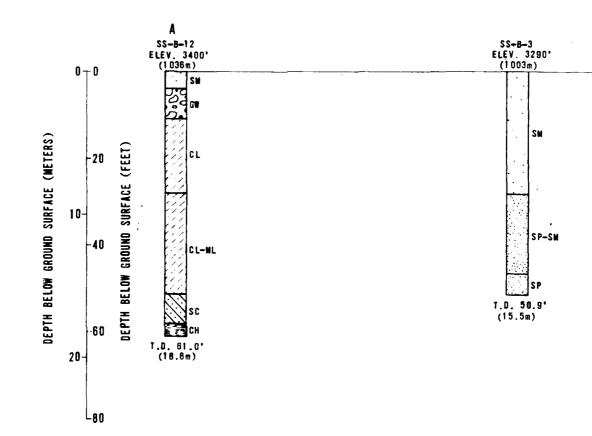
AL EXTE	NT (SITE)		PROPERTIE	SURFACE N					
(km ²)	PERCENT	GRADATION	CEMENTATION	MAXIMUM GRAIN SIZE	PAVEMENT/ PATINA	STAGE OF Caliche (c)	SLOPE (PERCENT)	DRAINAGE DEPTHS FEET (METERS)	NOTES
(48)	2	Poor- Moderately well	Weak- Moderate	Gravel	None/None	I-II	< 1	12-15 (4-5)	(d)
(24)	1	Poor	Strong	Boulder	None/None	П-Ш	< 1	0-5 (0-1.5)	
(172)	1	Poor	None-Weak	Sand	None /None	None	<u><</u> 1	0-5 (0-1.5)	
(737)	30	Poor	Weak-Strong	Cobble	None/None	I-III	1-2	10-15 (3-5)	(e)
(833)	35	Poor- Moderately well	None-Weak	Gravel	None/None	None-I	≤	0-2 (0-0 6)	(t)
(614)	25	Weli	Weak- Moderate	Boulder	Poor/Poor	None-III	1-3	0-6 (0-2)	(f)
							·		
						' '			

DESCRIPTION OF SURFICIAL
GEOLOGIC UNITS
SAN SIMON VALLEY, ARIZONA, HIGHLANDS CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SAMSO

TABLE

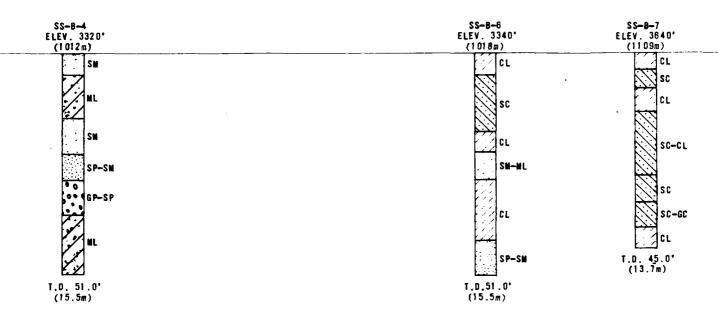
UGRO NATIONAL, INC.



NOTES: 1. Ground surface elevations :

2. T.D.=Total Depth

3. Soil types shown adjacent i (USCS) and are explained |

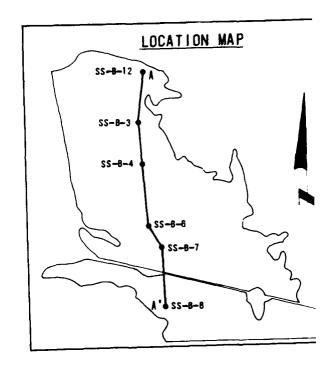


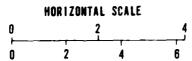
tions shown at locations of borings are approximate

acent to soil column are based on Unified Soil Classification System ained in the appendix

STATUTE MILES

KILOMETERS

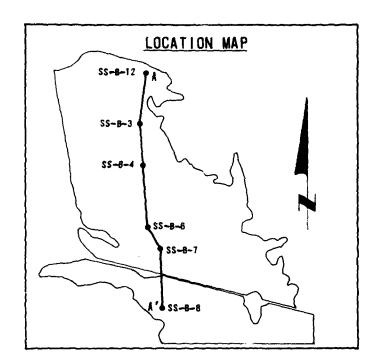




SOIL PROFILI SAN SIMON, AF HIGHLANDS

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE

UBRO NATIO

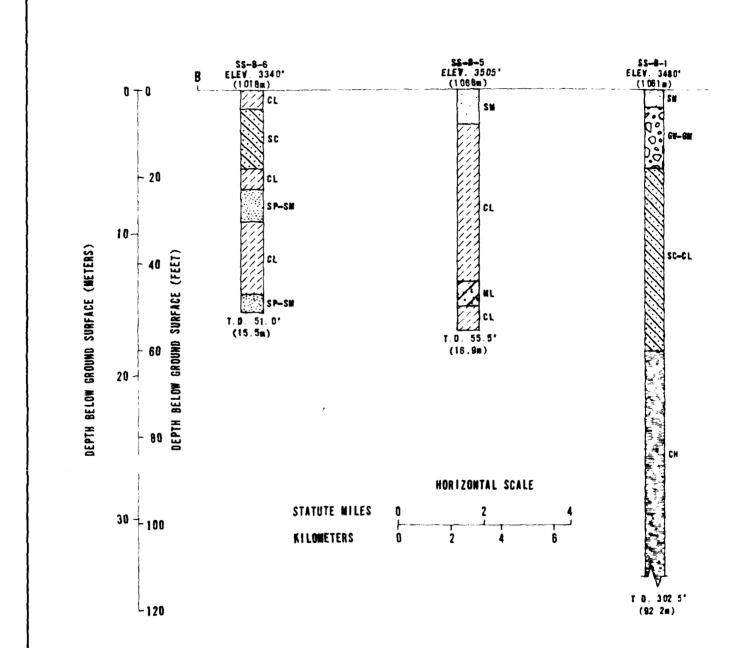


SOIL PROFILE AA" SAN SIMON, ARIZONA HIGHLANDS CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SAMSO

FIGURE 11

VERO NATIONAL INC.



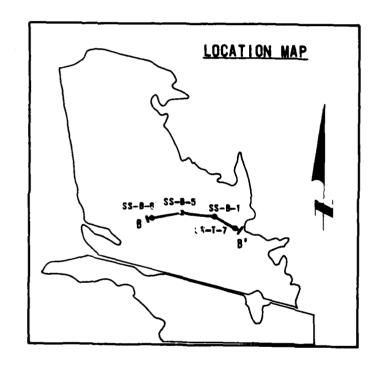
- NOTES: 1. Ground surface elevations shown at locations of borings are approximate
 - 2. T.B. = Total Depth
 - Soil types shown adjacent to soil column are based on Unified Soil Clas-(USCS) and are explained in the appendix

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2M 1) 180. \$\$-T-7 ELEV. 3700° (1128m) 0 + 0 GW-GM (3 1m) 20-- 10 DEPTH BELOW GROUND SURFACE (METERS) SC-CL DEPTH BELOW GROUND SURFACE (FEET) 40-60 -80-CH 100 - 30 120



proximate

Soil Classification System

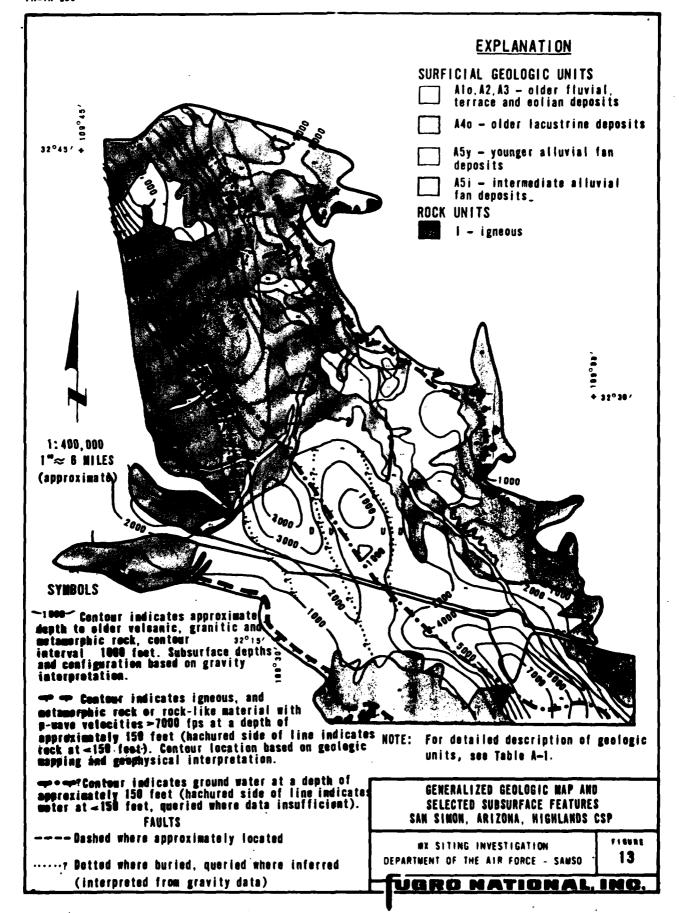
2

SOIL PROFILE BB° SAN SIMON VALLEY ARIZONA HIGHLANDS CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

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Ground water occurs at depths of less than 150 feet (46 m) over approximately 45 percent of the San Simon site. However, extrapolation of known data indicates shallow ground water may be encountered over an additional 20 percent of the site.

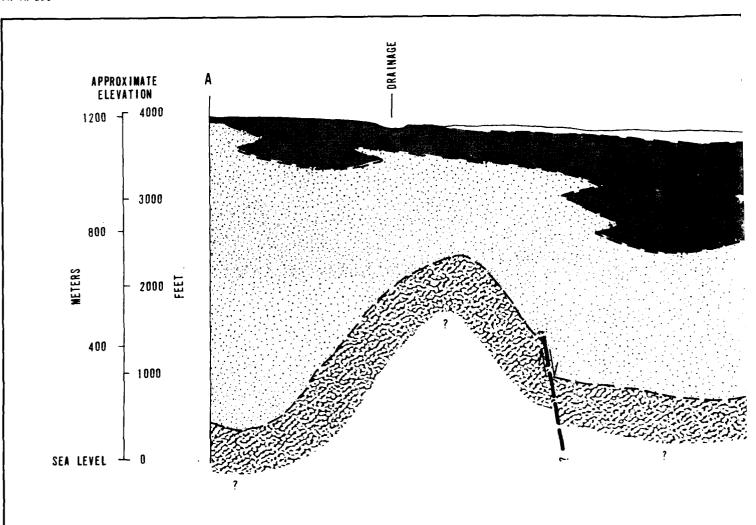
3.3.3 Basin Configuration

Results of the gravity survey were used to define the basin configuration (Figure 13). The basin appears to be a deep trough which has been uplifted and faulted in the central part of the valley (Figure 14). The trough is *proximately

deep (2130 m) in the southern portion. Steep gradients on both sides of the valley indicate that the basin is fault controlled. A section through the central portion of the valley perpendicular to the valley axis shows a horst-graben structure with a maximum depth of about 4500 feet (1377 m) in the graben. This structure is located in the uplifted area in the south-central portion of the trough. The subsurface basin configuration is illustrated in Figure 14.

3.4 GEOPHYSICAL PROPERTIES

Results of the shallow seismic refraction and electrical conductivity surveys are shown in Tables 14 and 15. Observed seismic velocities ranged from 1000 to 6330 fps (305 mps to 1930 mps). Surface layer velocities ranged from 1000 to 1440 fps (305 mps to 439 mps). This layer is 25 feet (8 m) thick, although it is typically about 5 feet (1.5 m) thick at other locations. Low velocity (<2000 fps; 610 mps) layers at SS-S-6 and 9 extend to



NOTES:

I The cross section is generally representative of subsurface conditions within the band shown on the location map. Due to the limited density of available data and the sparseness of new'y acquired data, the subsurface conditions are highly interpretive.

2. For a detailed description of geologic units see Table A-1.

<u>EXPLANATION</u>

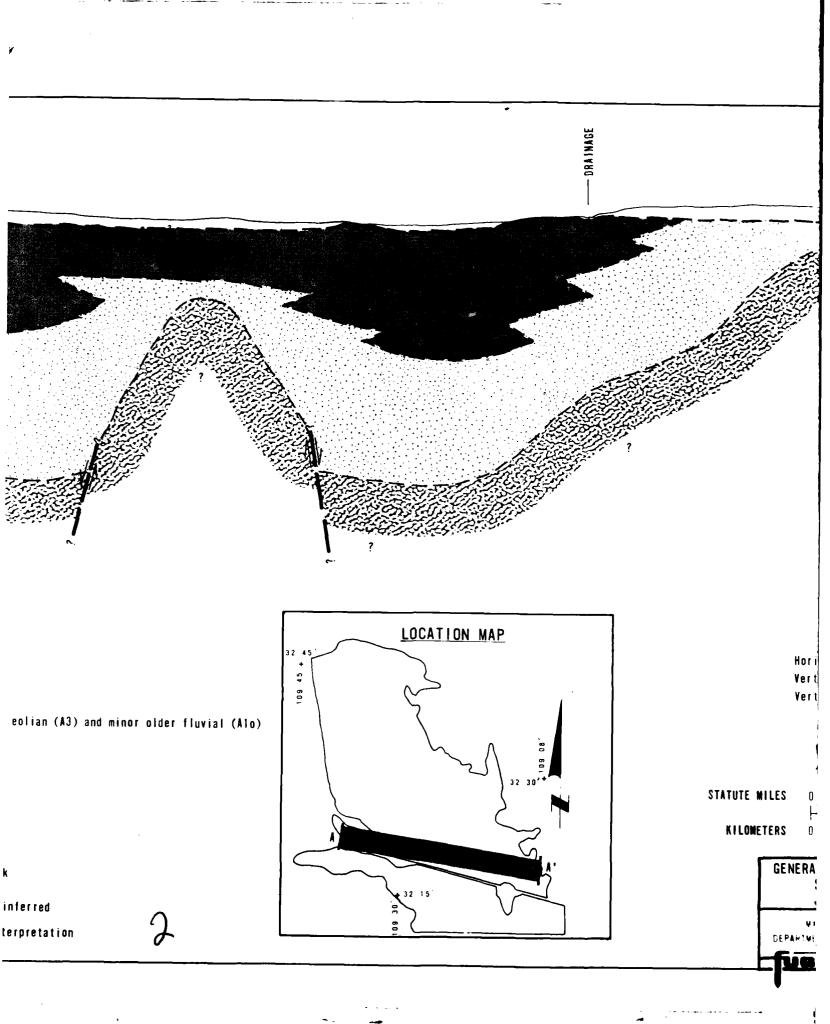
Undifferentiated basin-fill deposits

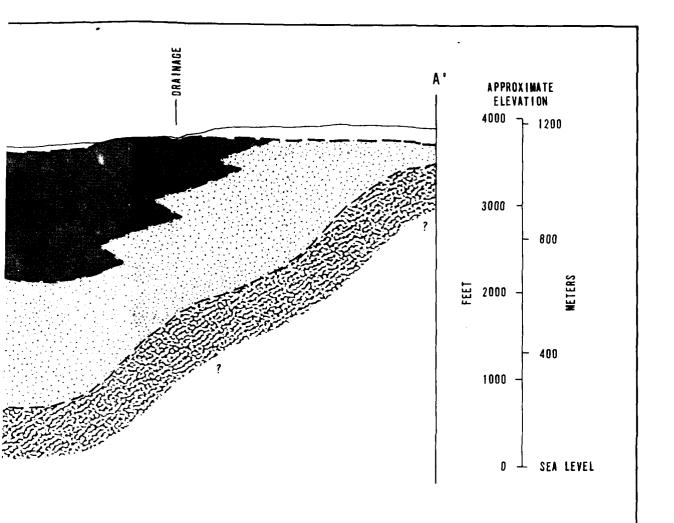
Predominantly alluvial (A5) deposits, with eolian (1 and stream terrace (A2) deposits

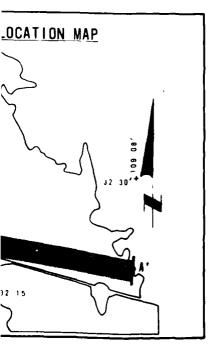
Older lacustrine (A4o) deposits

Undifferentiated older basin-fill deposits

Undifferentiated igneous and metamorphic rock

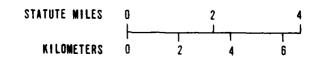






Horizontal Scale: 1 = 2 Miles (3 km) Vertical Scale: 1 = 1000 (305 m) Vertical Exaggeration: 10.5 X

HORIZONTAL SCALE



GENERALIZED GEOLOGIC CROSS SECTION
SAN SIMON VALLEY, ARIZONA
HIGHLANDS CSP

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE S

FIGURE 14

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S EXCLUSION DEPTH TO 7000 FPS (2134 MPS)	115 (35)	152 (46)	96 (29)	138 (42)	146 (45)	155 (47)	166 (51)	170 (52)	107 (33)	164 (50)	158 (48)	78 (24)			FEET (M)			7 1			
DEFRACTORS DEPTH VELOCITY	ŧ	ı	1	1	, 	ı	1	 	1	 	ì	,			FT (M)		0				
	A	A	A	A	A	A	A	A	A	A	A	A				45	0 150	16:36			
								4750 (1450)			(1670)					40	130 140				
		180)	6330 (1930)				1120)	4750			5480 (1670					35	120	1001/400			
	1	3880 (1180)	633			(830)	3690 (1120)	V			Ÿ						0110	ן נים			
(MPS)	(0)				(940)	3050	:	A	5540 (1690)	(880)	A	(1430)				30	06	edition of 1000 and the contract of the			
ON FPS	3990 (1220)		Y	20)	3100 (ļ			5540	2920 (890)		4680				25		+ 101001			
VELOCITY DISTRIBUTION FPS (MPS)	39	Y A		4000 (1220)		,	X	•								20	GO 70 80 Depth interval				
CITY DIS			(099)	4		Y A		6			0)					. •					
VELO		690)	2180 (6			^) QC	2420 (740)	,		2550 (780)	١				- 12	40 50	3 0 2 0			
		2280 (690)				(069)	2290 (700)	24	Å	X	21	* • •				≘-	30 4	distantant of an extension			
			v	v	Y	V		*	2260 (690)	72		90 (520)	(001)		1690 (520)				ro -	20	_
	<u>*</u>		1500 (460)		1400 (430)	y				2300 (<u> </u>			1000 (300)	<	<u>></u> - 0	If no refraction			
	1340 (410)	(340)	1050 (320)	2000 (610)	140	1440 (430)	1270 (390)	1300	(350)	1320 (400)	Y	1150 (350)			a 1000		- 52	-			
SEISMIC LINE NO.	1-8-88	SS-S-2	55-5-3) 4-S-SS	\$5-\$-\$	9-5-55	1-5-55	8-8-8	82-2-9	55-5-11	21-2-58	88-8-13				METERS 0	FEET O	•			
				., .						SH			IMON	VA		CTI	ON RE				
										DEPA			NG IN	/EST	IGATI	ON	IVS0	ī			

ACTIVITY LOCATION*	AVERAGE CONDUCTIVITY (mhos m)**
R-1	0.021
R-2	0.014
R-3	0.016
R-4	0.014
R-5	0.038
R-6	0.032
R-7	0.047
R~8	0.019
R-9	0.118
R-11	0.011
R-12	0.129
R-13	0.074

- *Resistivity was determined using a Schlumberger Array at each location where a seismic refraction survey was conducted.
- **Conductivity is the inverse of resistivity.

 Numbers presented are the average of values determined to a depth of 50 feet, computed as follows:

Average Conductivity = $(c_1t_1+c_2t_2+\ldots+c_nt_n)$ 50 feet

Whata

Average Conductivity = mhos/m

 t_1 through t_n = Thickness (feet) of layers 1 through n to 50 feet

CONDUCTIVITY SURVEY RESULTS SAN SIMON VALLEY, ARIZONA HIGHLANDS CSP

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depths of 40 feet (12 m). Average conductivities for the upper 50 feet (15 m) of soil are between 0.011 and 0.129 mhos/m.

3.5 ENGINEERING PROPERTIES

Laboratory tests were performed to determine the engineering properties of soil samples obtained from the various geologic units. The testing program consisted of classification, consolidation, shear strength, compaction, CBR and chemical. The range of engineering and geophysical properties of predominant geologic units is presented in Table 16.

Younger and intermediate alluvial fan deposits could not be differentiated at depth, and they were combined into one unit (A5) due to their similar grain size and engineering properties. These deposits consist predominantly of dense to very dense, silty and clayey sands, and gravels which are only slightly compressible and have high shear strengths.

Older lacustrine deposits were generally encountered at depths below alluvial fan deposits. These deposits are predominantly stiff to very stiff clays and silty clays near the valley interiors and coarse sandy gravels along the periphery. Clays and silty clays are expansive when saturated, only slighty compressible and have high shear strengths. Gravels are generally coarse to very coarse and mixed with cobbles and boulders which are relatively incompressible and have very high shear strengths.

The gradation ranges of the geologic units are shown in Figure 15. Table 17 shows the results of chemical tests on

ENGINEERING AND GEOPHYSICAL PROPERTIES	Younger and intermediate alluvial ran deposits (A5i and A5v)	Older lacustrine depo			
UNIFIED SOIL CLASSIFICATION SYMBOL(S)	SM. SC. GM. GC. GP. CL	CL, CH, ML, SH			
GENERAL PROPERTIES					
DRY DENSITY pcf(kg m ³)	90-122 (1442-1954)	85-117 (1362-18			
MOISTURE CONTENT (%)	2-28	2-30			
DEGREE OF SATURATION (")	25-85	14-90			
SPECIFIC GRAVITY	2.63-2.70	2 63-2 68			
DEGREE OF CEMENTATION	None to moderate	Weak to strong			
COMPRESSIONAL WAVE VELOCITIES fps(mps)	1000-4680 (305-1426)	1050-2920 (320-8			
ELECTRICAL CONDUCTIVITY (mhos m)	DNA	.005191			
GRAIN SIZE DISTRIBUTION (%)					
BOULDERS >12 inches(30cm)	0-10	0			
COBBLES 3 to 12 inches(8to 30cm)	0-25	0-5			
GRAVEL	0-55	0-20			
SAND	0-90	0-88			
SILT AND CLAY	10-97	0-98			
PLASTICITY DATA					
LIQUID LIMIT	19-72	26-84			
PLASTICITY INDEX	NP-44	NP-60			
COMPRESSIBILITY DATA					
COMPRESSION AT 4 ksf(192kN/m²) (2)	0.8-2.3	0.5-1 6			
SWELL OR COLLAPSE UPON SATURATION (%)	0.2-1.4(Swell)	0 3-1 2 (S			
SHEAR STRENGTH DATA					
UNCONFINED COMPRESSION ksf(kn/m²)	2.0-6.9 (96-330)	3.6-34.4 (172-16			
CD TRIAXIAL COMPRESSION	DNA	c =1-3 ksf(48-144 kN m ²)			
DIRECT SHEAR ksf(kn/m²)	D. 4-5.7 (19-273)	0.4-3.7 (19-17			
COMPACTION AND CBR DATA					
MAXIMUM DRY DENSITY pcf(kg m ³)	118-135 (1890 -2162)	115-126 (1842-20			
OPTIMUM MOISTURE CONTENT (*)	9.8-12.5	10.5-15.8			
CBR AT 90% RELATIVE COMPACTION	20-30	6-9			

DNA = DATA NOT AVAILABLE (INSUFFICIENT DAJA OR TESTS NOT PERFORMED)

GEOLOG	IC UNITS
acustrine deposits (A4o)	
CL. CH. ML. SW. SP	
85-117 (1362-1874)	
2-30	
14-90	
2.63-2.68	
Weak to strong	
50-2920 (320 - 890)	
.005191	
0	
0-5	
0-20	
0-88	
0-98	
26-84	
NP-60	
0 5-1 6	
0 3-1 2 (Swell)	
-34.4 (172-1647)	
$8-144 \text{ kN m}^2$), $\phi = 12^{\circ}-25^{\circ}$	
1.4-3.7 (19-177)	· · · · · · · · · · · · · · · · · · ·
-126 (1842-2018)	
10.5-15.8	
6-9	

RANGE OF ENGINEERING
AND GEOPHYSICAL PROPERTIES
SAN SIMON VALLEY, ARIZONA, HIGHLANDS CSP

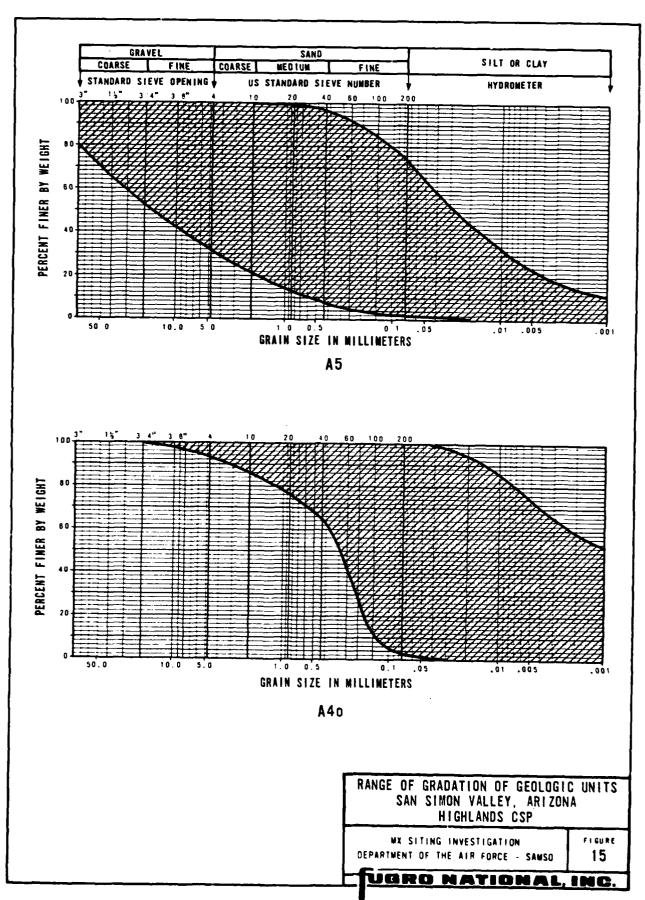
MX SITING INVESTIGATION

TABLE

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_		_	_							 						
CALCIUM	CALCIUM		1510	613	1950	180	478	121								
u	CALCIUM	mg/kg	1740	320	530	80	118	75					ï			
WATER SOLUBLE	SULPHATE	mg/kg	820	1020	920	560	370	640			_					
Y X	CHLORIDE	mg/kg	28	670	2670	230	18	200								
	SODIUM	mg/kg	1440	080	1420	890	470	540								
Γ	蓋		7.9	8.4	7.7	7.8	6.3	7.2								
	SOIL TYPE		HM-HJ	MI	#S	כו-אור	NS.	dS								
MTCDVAI	MICHVAL	METERS	6.10-6.31	6.10-6.25	6.10-8.25	3.05-3.50	0.76-1.37	3.05-3.81								
	SAMPLE INIERFAL	FEET	20.0-20.7	20.0-20.5	20.0-20.5	10.0-11.5	2.5-4.5	10.0-12.5								
	SAMPLE		I	0-5	0-5	B3	ī	8-2								
	BORING / STRENCH		SS-B-1	SS-B-4	8S-B-8	1-1-55	7-1-SS	SS-T-6	_							

SUMMARY OF CHEMICAL TEST RESULTS SAN SIMON VALLEY, ARIZONA HIGHLANDS CSP

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO

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soil samples and they indicate that sulfate attack potential of soil on concrete is generally "negligible."

Logs of three representative borings and trenches are shown in Appendix C. Results of shear strength and CBR tests performed on soil samples from the site and a summary of all the laboratory tests performed on soil samples from boring SS-B-l are also included in Appendix C.

4.0 DISCUSSION

4.1 JORNADA DEL MUERTO SITE

Based on regional geologic information, geotechnical conditions of the Jornada Del Muerto site are generally representative of approximately 95 percent of the Rio Grande CSP and are summarized below:

- o The eolian sheet sand, younger alluvial fan deposits, and intermediate alluvial fan deposits are the predominant surficial geologic units. (Eolian sheet sand is the most dominant).
- o Older lacustrine material is predominant within the construction zone (150 ft; 46 m).
- o The site area is generally a structural basin bounded by a potentially active fault on the east.
- o The terrain slopes gently towards closed central basin areas.

4.2 SAN SIMON SITE

Based on regional geologic information, geotechnical conditions of the San Simon site are generally representative of approximately 40 percent of the Highlands CSP and are summarized below.

- o The younger alluvial fan deposits, intermediate alluvial fan deposits and older lacustrine deposits are the predominant surficial geologic units (the younger alluvial fan deposits are the most dominant).
- o The site area is generally a down-dropped structural block (graben) bounded by potentially active faults.
- o The terrain slopes gently towards open central valleys.

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5.0 CONSTRUCTION CONSIDERATIONS

In this section geotechnical factors and conditions applicable to construction of the MX system are discussed. The three basing mode concepts presently considered are vertical shelter, in-line hybrid trench, and horizontal shelter. The important geotechnical factors for a vertical shelter are primary, secondary and interconnecting roads, excavation of shelters, and drainage crossings. For the in-line hybrid trench, important geotechnical factors are excavation and backfill, roads (primary, secondary, and temporary), drainage crossings, and aggregates for roads and concrete. For the horizontal shelter, roads and drainage crossings are the important geotechnical factors. A summary of the applicable geotechnical factors is presented in the following paragraphs:

- o Terrain Surficial slopes are typically less than one percent, requiring little preconstruction grading for roads and trenches. Depths of drainage incision are generally less than ten feet (3 m) minimizing the need for major drainage structures for roads and trenches. However, in the northeastern portion of San Simon Site depths of drainage incision are ten feet (3 m) or greater requiring major drainage structures.
- o Roads A good network of paved and unpaved roads exists at the Jornada Site. However, no regular network of paved or unpaved roads exists at the San Simon site.

 Therefore, a network of new roads will be required.

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Most of the surficial soils at both the sites have good to excellent subgrade characteristics when compacted, resulting in economical road sections. In approximately 25 percent of the Jornada site the surficial soils do not have good support characteristics for use as road subgrade, thus requiring thicker, more costly road sections.

o Excavation - Most of the subsurface soils are dense, weakly to moderately cemented, and possess moderately high shear strength. Except in areas close to mountain fronts, compressional wave velocities range from 1000 to 6000 fps (305 to 1830 mps) up to depths of 150 feet (46 m) below ground surface, indicating good excavatability. The soils are suitable for excavation of: vertical shelters by augers, continuous trenches (castin-place trench construction) by an MX trencher, and horizontal shelters using conventional equipment. In approximately 20 percent of the Jornada site, vertical walls of excavations for trenches and vertical shelters may be unstable, requiring additional expense for other excavation techniques. Approximately five percent of the area of the two sites has zones of concentrated cobbles and boulders where an MX trencher will not be able to excavate a trench suitable for cast-in-place construction.

Depth to rock is greater than 150 feet (46 m) over a major portion of the sites, therefore, additional

expense for excavation of vertical shelters is minimal. Depth to ground water is less than 150 feet (46 m) in approximately 30 and 65 percent of Jornada and San Simon sites, respectively. In areas where the depth to ground water is less than 120 feet (37 m), additional costs for excavation of vertical shelters can be expected.

- o Backfill Subsurface soils are generally suitable for backfill and compaction in trench excavations. Backfill will have to be imported from within the sites for areas of concentrated cobbles and boulders.
- o Aggregates and Water Sufficient quantities of aggregates and water required for roads and concrete of all basing modes are available within and/or adjacent to the sites, thus minimizing haul costs.

6.0 CONCLUSIONS

In summary, Jornada del Muerto and San Simon sites present favorable geotechnical conditions for deployment of any of the three present MX basing mode concepts. For the vertical shelter basing mode, cost of excavation for vertical shelters will be high in many areas due to the presence of ground water within the construction zone. As an alternative, areas with ground water in the construction zone can be excluded for the vertical shelter mode. Geotechnical conditions from the Jornada and San Simon sites can be extrapolated to approximately 95 and 40 percent of the Rio Grande and Highlands CSPs, respectively.

APPENDIX A
GENERAL GEOTECHNICAL INFORMATION

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TEXT

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GLOSSARY OF TERMS

- ACTIVITY NUMBER A designation composed of the valley abbreviation followed by the activity type and a unique number; may also be used to designate a particular location in a valley.
- AEROMAGNETIC DATA Magnetometer observations made from an airplane.
- ALLUVIAL BASIN A lowland area, generally between uplifted mountain blocks, filled with alluvial deposits.
- ALLUVIAL FAN A low, outspread, relatively flat to gently sloping mass of alluvium, shaped like an open fan or a segment of a cone, deposited by a stream (especially in a semiarid region) at the place where it issues from a narrow mountain valley upon a plain or broad valley. It is steepest near the mouth of the valley where its apex points upstream, and it slopes gently and convexly outward with gradually decreasing gradient.
- ALLUVIAL FAN DEPOSITS Alluvium deposited by a stream or other body of running water as a sorted or semisorted sediment in the form of a cone or fan at the base of a mountain slope.
- ALLUVIAL PLAIN A level or gently sloping tract or a slightly undulating land surface produced by extensive deposition of alluvium, usually adjacent to a river that periodically overflows its banks; it may be situated on a flood plain, a delta, or an alluvial fan.
- ALLUVIUM A general term for unconsolidated clay, silt, sand, gravel, and boulders deposited during relatively recent geologic time by a stream or other body of running water as a sorted or semisorted sediment in the bed of a stream or on its flood plain or delta, or as a cone or fan at the base of a mountain slope.
- ANOMALY 1) A deviation from uniformity in physical properties; especially a deviation from uniformity in physical properties of exploration interest. 2) A portion of a geophysical survey which is different in appearance from the survey in general.
- AQUIFER A permeable saturated zone below the earth's surface capable of conducting and yielding water as to a well.

- ARKOSIC SANDSTONE A sandstone with considerable feldspar, such as one containing minerals from coarse-grained quartzo-feldspathic rocks (granites, granodiorites, medium or high-grade schists) or from older, highly feldspathic sedimentary rocks; specifically a sandstone containing more than 25% feldspar and less than 20% matrix material of clay, sericite, and chlorite.
- ARRIVAL An event; the appearance of seismic energy on a seismic record; a line-up of coherent energy signifying the arrival of a new wave train.
- ATTERBERG LIMITS A general term applied to the various tests used to determine the various states of consistency of fine grained soils. The four states of consistency are solid, semisolid, plastic, and liquid.

Liquid limit (LL) - The water content corresponding to the arbitrary limit between the liquid and plastic states of consistency of a soil (ASTM D423-66).

Plastic limit (PL) - The water content corresponding to an arbitrary limit between the plastic and the semisolid states of consistency of a soil (ASTM D424-59).

Plasticity index (PI) - Numerical difference between the liquid limit and the plastic limit.

- BASIN-FILL MATERIAL/BASIN-FILL DEPOSITS Heterogenous detrital material deposited in a sedimentary basin.
- BEDROCK Rock with a seismic p-wave velocity of 7000 ft (2333 m) per second or more.
- BOUGUER ANOMALY The residual value obtained after latitude, elevation and terrain corrections have been applied to gravity data.
- BOULDER FIELD Five or more rocks, each with diameters of 6 ft or more occurring within an acre.
- BULK SAMPLE A disturbed soil sample (bag sample) obtained from cuttings brought to the ground surface by a drill rig auger or obtained from the walls of a trench excavation.
- c Cohesion (Shear strength of a soil not related to interparticle friction).
- CALICHE Gravel, sand or other material cemented principally by calcium carbonate.

- CALIFORNIA BEARING RATIO (CBR) A test performed on a specifically prepared soil sample which is useful in the design of road pavement to be supported by the soil tested (ASTM D1833-73). The load is applied on the penetration piston which is penetrated into the soil sample at a constant penetration rate. The bearing ratio reported for the soil is normally the one at 0.1 inches (2.5 mm) penetration.
- CANDIDATE One of some group of regions, areas or sites being considered for MX deployment. Removal of candidate from a specifically named region, area or site term indicates selection by SAMSO/MNND.
- CANDIDATE DEPLOYMENT AREA (CDA) An area encompassing between 500 and 1000 square nautical miles of potentially suitable land with either naturally or artificially defined boundaries designated for convenience of study, discussion and data depiction. The candidate deployment area could be composed of two to four parcels and should have a specific place name description.
- CANDIDATE DEPLOYMENT PARCEL (CDP) An area of 150 to 500 square nautical miles potentially suitable for MX siting which, when aggregated with others, forms a Candidate Deployment Area. Each parcel should have a specific geographic description. (In the Basin and Range Physiographic province a parcel may correspond to a geographic valley and in Texas to some agri-economic unit.)
- CANDIDATE DEPLOYMENT SITE (CDS) A non-specific (i.e. not finally approved) site proposed for some element of the MX system within a chosen deployment area (i.e. trench or shelter site).
- CANDIDATE SITING PROVINCE (CSP) An area potentially suitable for deployment of the MX system generally encompassing more than 6000 square nautical miles which, in a broad sense, is homogeneous with respect to most of the important characteristics governing siting of a total MX system.
- CANDIDATE SITING REGION (CSR) Potentially suitable area between 4000 and 6000 square nautical miles within one, or encompassing portions of more than one, candidate siting province which allows for full MX deployment.

- CAPABLE (fault) Movement at or near the surface at least once in the past 35,000 years, and/or more than once in the past 500,000 years, (Nuclear Regulatory Commission).
- CAPROCK A resistant, moderately to strongly cemented caliche layer forming a "cap" over less resistant layers.
- CD TRIAXIAL SHEAR-A type of test to measure the shear strength of an undisturbed soil sample
- CLOSED BASIN A catchment area draining to some depression or lake within its area, from which water escapes only by evaporation.
- COARSE-GRAINED A term which applies to a soil of which more than one-half of the soil particles, by weight, are larger than 0.075 mm in diameter (passing the No. 200 U.S. size).
- COARSER-GRAINED A term applied to alluvial fan deposits which are predominantly composed of material larger than 3 inches (76 mm) in diameter.
- COLLUVIAL DEPOSITS A general term applied to any loose, heterogenous, and incoherent mass of soil material or rock fragments deposited chiefly by dislodgement and downslope transport of the material under the direct application of gravitational body stresses. Material is usually found at the base of a steep slope or cliff.
- COMPACTION TEST A type of test to determine the relationship between the moisture content and density of a soil sample which is prepared in compacted layers at various water contents (ASTM D1557-70).
- COMPRESSIBILITY-Property of a soil pertaining to its susceptibility to decrease in volume when subjected to load.
- COMPRESSIONAL WAVE -An elastic body wave in which particle motion is in the direction of propagation; the type of seismic wave assumed in conventional seismic exploration. Also called P-wave, dilatational wave, and longitudinal wave.
- CONSOLIDATION TEST A type of test to determine the compressibility of a soil sample. The sample is enclosed in the consolidometer which is then placed in the loading device. The load is applied in increments at certain time intervals and the change in thickness is recorded.

- CONTERMINOUS UNITED STATES The contiguous 48 states.
- CORE SAMPLE A cylindrical sample obtained with a rotating core barrel with a cutting bit at its lower end. Core samples are obtained from indurated deposits and in rock.
- DEBRIS FLOW A high-density flow of mud containing abundant coarse-grained materials (boulders, cobbles, gravel, sand) that frequently result from an unusually heavy rain.
- DEGREE OF SATURATION Ratio of volume of water in soil to total volume of voids.
- DETECTOR See GEOPHONE.
- DIRECT SHEAR TEST A type of test to measure the shear strength of a soil sample where the sample is forced to fail on a predetermined plane.
- DISSECTION/DISSECTED (alluvial fans) The cutting of stream channels into the surface of an alluvial fan by the movement (or flow) of water.
- DISTAL That portion of an alluvial deposit farthest from its point of origin.
- DRY UNIT WEIGHT/DRY DENSITY Weight per unit volume of the solid particles in a soil mass.
- ELECTRICAL CONDUCTIVITY Ability of a material to conduct electrical current
- ELECTRICAL RESISTIVITY Property of a material which resists flow of electrical current
- EOLIAN A term applied to materials which are deposited by wind.
- EPHEMERAL(stream) A stream in which water flow is discontinuous and of short duration.
- EXTERNAL DRAINAGE Stream drainage system whose downgradient flow is unrestricted by any topographic impediments.
- EXTRUSIVE (rock) Igneous rock that has been ejected onto the earth's surface (e.g., lava, basalt, rhyolite, andesite; detrital material, volcanic tuff, pumice).

- FAULT A plane or zone of rock fracture along which there has been displacement.
- FAULT BLOCK MOUNTAINS Mountains that are formed by normal faulting in which the surface crust is divided into structural, partially to entirely fault-bounded blocks of different elevations.
- FINE-GRAINED A term which applies to a soil of which more than one-half of the soil particles, by weight, are smaller than 0.075 mm in diameter (passing the No. 200 U.S. size sieve).
- FINER-GRAINED A term applied to alluvial fan deposits, which are composed predominantly of material less than 3 inches (76 mm).
- FLOODING/LOW ENERGY FLOW Flood waters flowing on a slope of low gradient.
- FLUVIAL DEPOSITS Material produced by river action; generally loose, moderately well-graded sands and gravel.
- FORMATION A mappable assemblage of rocks characterized by some degree of homogeneity or distinctiveness
- FREE AIR ANOMALY Gravity data which have been corrected for latitude and elevation (free air correction) but not for the density of rock between the datum and the plane of measurement (Bouguer correction).
- FUGRO DRIVE SAMPLE A 2.50 inch (6.4 cm) diameter soil sample obtained from a drill hole with a Fugro Drive Sampler. The Fugro drive sampler is a ring-lined barrel sampler containing 12 one-inch (2.54 cm) long brass sample rings. The sampler is advanced into the soil using a drop-hammer.
- GAMMA A unit of magnetic-field intensity. A gamma is 10^{-5} oersteds; sometimes expressed (incorrectly) as 10^{-5} gauss with which it is numerically equal.
- GEOMORPHOLOGY The study, classification, description, nature, origin, and development of present landforms and their relationships to underlying structures, and of the history of geologic changes as recorded by these surface features.
- GEOPHONE The instrument used to transform seismic energy into electrical voltage; a seismometer, jug, or pick-up.

- GRAIN-SIZE ANALYSIS (GRADATION) A type of test to determine the distribution of soil particle sizes in a given soil sample. The distribution of particle sizes larger than 0.075mm (retained on the No. 200 sieve) is determined by sieving, while the distribution of the particle sizes smaller than 0.075 mm is determined by a sedimentation process, using a hydrometer.
- GRAVEL Particles of rock that pass a 3-in. (76.2 mm) sieve and retained on a No. 4(4.75 mm0 sieve
- GRAVITY The force of attraction between bodies because of their mass. Usually measured as the acceleration of gravity.
- GRAVITY GRADIENT The partial derivative of the acceleration of gravity with respect to distance in a particular direction, for which purpose the acceleration of gravity is considered as a scalar.
- INTERIOR DRAINAGE Stream drainage system that flows into a closed topographic low (basin).
- LACUSTRINE DEPOSITS Materials deposited in lake environment.
- LINE A linear array of observation points, such as a seismic line.
- LIQUID LIMIT See ATTERBERG LIMITS.
- LOESS A wind blown deposit predominantly silt or silty clay or clayey silt.
- LOW ENERGY FLOW See FLOODING.
- MAGNETIC INTENSITY A vector quantity measuring magnetic field strength. The unit of magnetic intensity commonly used in geophysical exploration is the gamma (see GAMMA).
- MANTLED PLAYA A playa surface or a portion of the surface that is covered with younger geologic material such as windblown sand, or alluvium.
- MILLIGAL A unit of acceleration used with gravity measurements; 1 milligal = 10^{-5} m/sec.². Abbreviated mgal.

§ .

- MOISTURE CONTENT The ratio, expressed as a percentage, of the weight of water contained in a soil sample to the oven-dry weight of the sample.
- N VALUE Penetration resistance, number of blows required to drive the standard split spoon sampler for the second and third six inches (0.15 m) with a 140 pound (63.5 kg) hammer falling 30 inches (0.76 m) (ASTM D1586-67).
- OPTIMUM MOISTURE CONTENT Moisture content at which a soil can be compacted to a maximum dry unit weight by a given compactive effort
- OVERBANK FLOODING A large flow of water that overflows the sides of A stream channel.
- O Angle of internal friction
- PATINA A dark coating or thin outer layer produced on the surface of a rock or other material by weathering after long exposure (e.g., desert varnish).
- PAVEMENT/DESERT PAVEMENT When loose material containing pebble-sized or larger rocks is exposed to rainfall and wind action the finer dust and sand are blown or washed away and the pebbles gradually accumulate on the surface, forming a mosaic which protects the underlying finer material from wind attack. Pavement can also develop in finer-grained materials. In this case the armored surface is formed by dissolution and cementation of the grains involved.
- PEGAMATITE DIKE A coarse grained igneous rock of granitic composition that forms as a tabular intrusion that cuts across the planar structures of the surrounding rock.
- P-WAVE See COMPRESSIONAL WAVE.
- PERIMETER SEISMIC REFRACTION SURVEY Shallow seismic refraction measurements made around the perimeter of a valley.
- PERMEABLE The ability of liquid to pass through soil and/or rock material.
- PICK-UP See GEOPHONE.

PITCHER TUBE SAMPLE - An undisturbed, 2.87 inch (73 mm) diameter soil sample obtained from a drill hole with a Pitcher tube sampler. The primary components of this sampler are an outer rotating core barrel with a bit and an inner stationary, spring-loaded, thin-wall sampling tube which leads or trails the outer barrel drilling bit, depending upon the hardness of the material being penetrated.

PLASTIC LIMIT - See ATTERBERG LIMITS.

PLASTICITY INDEX - See ATTERBERG LIMITS.

- PLAYA/PLAYA DEPOSITS A term used in the southwest U.S. for a dried-up, flat-floored area composed of thin, evenly stratified sheets of fine clay, silt, or sand, and representing the lowest part of a shallow, completely closed or undrained, desert lake basin in which water accumulates and is quickly evaporated, usually leaving deposits of soluble salts.
- PONDING (of water) The accumulating of water in a topographic depression.
- PRIME Modifier used to indicate the highest ranking province, region, area, or site. If not an interdisciplinary ranking, then a qualifier should be used such as "prime" geotechnical candidate siting area".
- PROXIMAL That portion of an alluvial deposit nearest to its point of origin.
- REGIONAL The general attitude or configuration disregarding features smaller than a given size. The regional gravity is the gravity field produced by large-scale variations ignoring anomalies of smaller size. See residualize.
- RELATIVE AGE The relationship in age (oldest to youngest) between geologic units without specific regard to number of years.
- RESIDUAL What is left after a regional field has been removed, as in gravity or magnetic analysis. See RESIDUALIZE.

- RESIDUALIZE The process of separating a graphically depicted curve or a surface into its low-frequency parts (called the regional) and its high-frequency parts (called the residual). Residualizing is an attempt to sort out of the total field those anomalies which result from local structure; that is, to fine local anomalies by subtracting gross (regional) effects.
- ROCK UNITS Distinct rock masses with different characteristics (e.g., igneous, metamorphic, sedimentary).
- S-WAVE See SHEAR WAVE.
- SAND Soil passing through No. 4(4.75 mm) sieve and retained on No. 200 (0.075 mm) sieve
- SAND DUNE A low ridge or hill consisting of loose sand deposited by the wind, found in various desert and coastal regions and generally where there is abundant surface sand.
- SEISMIC Having to do with elastic waves. Energy may be transmitted through the body of an elastic solid as P-waves (compressional waves) or S-waves(shear waves).
- SEISMIC REFRACTION DATA: deep/shallow Data derived from a type of seismic shooting based on the measurement of seismic energy as a function of time after the shot and of distance from the shot, by determining the arrival times of seismic waves which have travelled nearly parallel to the bedding in high-velocity layers, in order to map the depth to such layers.
- SEISMOGRAM A seismic record.
- SEISMOMETER See GEOPHONE.
- SHEAR WAVE A body wave in which the particle motion is perpendicular to the direction of propagation. Also called S-Wave or transverse wave.
- SHEET FLOW A process in which storm-borne water spreads as a thin, continuous veneer (sheet) over a large area.
- SHEET SAND A blanket deposit of sand which accumulates in shallow depressions or against rock outcrops, but does not have characteristic dune form.
- SHOT Any source of seismic energy; e.g., the detonation of an explosive.

- SHOT POINT The location of any source of seismic energy; e.g., the location where an explosive charge is detonated in one hole or in a pattern of holes to generate seismic energy. Abbreviated SP.
- SILT AND CLAY Fine-grained soil passing through No. 200 (0.075 mm) sieve.
- SITE Location of some specific activity or reference point.

 The term should always be modified to a precise meaning or be clearly understood from the context of the discussion.
- SPECIFIC GRAVITY The ratio of the weight in air of a given volume of soil solids at a stated temperature to the weight in air of an equal volume of distilled water at a stated temperature.
- SPLIT SPOON SAMPLE A disturbed sample obtained with a split spoon sampler with an outside diameter of 2.0 inches (5.1 cm). The sample consists of a split barrel which is driven into the soil using a drop-hammer.
- SPREAD The layout of geophone groups from which data from a single shot are recorded simultaneously. Spreads containing twenty-four geophones have been used in Fugro's seismic refraction surveys.
- STREAM CHANNEL DEPOSITS Materials (clay, silt, sand, gravel, cobbles, boulders) which have been deposited in a stream channel.
- STREAM TERRACE DEPOSITS Stream channel deposits no longer part of an active stream system, generally loose, moderately well graded sand and gravel.
- SURFICIAL DEPOSIT Unconsolidated residual and alluvial deposits occurring on or near the earth's surface.
- TRANSITORY A poorly defined, shallow ephemeral stream across an alluvial fan surface, the position of which is temporary and tends to shift frequently.
- UNIFIED SOIL CLASSIFICATION SYSTEM (USCS) A system which determines soil classification on the basis of grain-size distribution and Atterberg Limits. (See page A-17).

- VALLEY SEISMIC REFRACTION SURVEY Deep seismic refraction measurements made near the middle of a valley to determine seismic wave propagation velocities and thickness of basin fill.
- VELOCITY Refers to the propagation rate of a seismic wave without implying any direction. Velocity is a property of the medium and not a vector quantity when used in this sense.
- VELOCITY LAYER A layer of rock or soil with a homogenous seismic velocity.
- VELOCITY PROFILE A cross-section showing the distribution of material seismic velocities as a function of depth and its configuration.
- WASH SAMPLE A sample obtained by screening the returned drilling fluid during rotary wash drilling to obtain lithologic information between samples.

Definitions were derived in part from Webster's New Collegiate Dictionary (1972 edition), Glossary of Geology (American Geological Institute, 1972), Encyclopedic Dictionary of Exploration Geophysics (Sheriff, 1973), and 1976 Annual Book Book of ASTM Standards.

BIAGNOSTIC CARBONATE MORPHOLOGY

STAGE	GRAVELL	Y SOILS		NO	NGRAVELLY SDILS
1	Thin, disconti	nuous pebble	coatings	Few filam	ents or faint coatings
п	Continuous peb interpebble fi		, some	Few to abundant nodules, flakes, filaments Many nodules and internodular fillings Laminar horizon overlying plugged horizon	
ш	Many interpebb	le fillings			les and internodular
IJ	Laminar horizo horizon	n overlying p	olugged		orizon overlying plugged
	STAGE	I Weak Ca	II Strong Ca		
	GRAVELLY SOILS				K22 m
	NONGRAVELLY SOILS	****			K22m
	NONGRAVELLY SOILS	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$			

Stages of development of a caliche profile with time. Stage I represents incipient carbonate accumulation, followed by continuous build-up of carbonate until, in Stage IV, the soil is completely plugged.

SUMMARY OF CALICHE DEVELOPMENT

Reference: Gile, L.H. Peterson, F.F., and Grossman, R.B., 1965. The K. horizon: A master horizon of carbonate

accumulation: Soil Science, v. 99, p. 74-82

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SAMSO

A-1

ugro national, inc.

(1) AREI SYMBOLS	MX (2) GEOLOGIC UNITS	NON-ROCK UNITS	(1) AREI Symbols	MX (GEOLOGIC UNITS
Au. Ast	Au	Non-rock Deposits (undifferentiated); fine- to coarse-grained materials deposited by alluvial, fluvial, eclian, lacustrine, gravity or glacial processes.		
Aal	A 1	Fluvial Deposits; predominantly composed of poorly- to well-graded sand and gravel with lesser amounts of silt- and boulder-sized material. The unit predominantly consists of recent water-laid deposits occupying present drainages and flood plains.	gr	I
	-	Older Fluvial Deposits (Alo) are generally thicker, more extensive units deposited in ancestral fluvial systems.	٧u	
	-	Alluvial Outwash Deposits (Alw) consist of mixed, geomorphically nondescript alluvial and fluvial deposits covering large, relatively flat, river and playa basins.	٧b	
A t	A 2	Terrace Deposits; predo notify composed of moderately to well graded, clay— to gravel—sized material or capally elevated terraces bordering modern streams (A2s) and lakes playas (A21).	Su	S
	A3	Eclian Deposits; predominantly composed of poorly graded sand-sized material deposited by wind action. Deposits may consist of mixed sand, silt, and clay (A3u), or be differentiated on the basis of predominant grain size and landform.	Q tz ,	.
		A3s d - Predominantly fine sand-sized material deposited in sheets (A3s) or dunes (A3d). A31 - Loess composed predominantly of silt-sized material with lesser amounts	Psa. Pm Ph. Cau Ls. Py. Par	
		of clay and fine sand. A3f — Predominantly clay—sized material with lesser amounts of silt and fine sand.		_
	A4	Lacustrine, Estuarine, and Playa Deposits; predominantly composed of poorly graded clay, silt, and fine sand deposited in bodies of standing water. Older lacustrine, estuarine, and playa deposits (A4o) are thicker, more extensive units occupying ancestral lake basins.	Qtz. gn	M
Aaf	A 5	Alluvial Fan Deposits; predominantly composed of well graded sand and gravel with varying amounts of silt-, cobble-, and boulder-sized material. Deposited principally by distributary channels adjacent to mountain fronts. Relative ages are indicated by o - older, i - intermediate, or y - younger.		C
	A 6	Pediment, Pediment Deposits, and Areas of Shallow Rock; planated bedrock shelf or near surface rock generally overlain by a thin mantle of sand- to boulder-sized residual or alluvial material.		
	A7	Colluvial Deposits; predominantly composed of moderately- to well-graded sand and gravel with varying amounts of silt-, cobble-, and boulder-sized material.		

NOTES: (1) ARE1 symbols were developed for use in the Aggregate Resources Evaluation Investigation (See Section 5.1 and Drawings 5.1A through 5.1C)

Deposited locally by gravity and water adjacent to steep gradients.

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Show rock type IGNE part

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Modi (cal A3s A5y(\$5to

⁽²⁾ MX Geologic units were used for Methodology, Screening, and Characterization studies.

(1) MX (2)
AREI GEOLOGIC
SYMBOLS UNITS

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ROCK UNITS

Shown in regions where rock is expose; the areally predominant (greater than 70 percent) rock type is indicated. In those are some rock types occur the predominant rock type as shown followed by the subord are rock type (e.g. S2MP 14T).

- IGNEOUS (UNDIFFERENTIATED). Rocks formed by solidification of a molten or partially molten mass.
 - Intrusive Typically crystalline, formed by the solidification of molten material below the surface (e.g., granite, syenite, diorite).
 - Extrusive (undifferentiated). Formed by solidatication of molten material at or near the surface.
 - Extrusive (flows). Extrusive rocks formed by solidification of lava (e.g. basalt, dacite) in menotes young basaltic flows which may be interbedded with basis of materials.
 - Extrusive (volcaniclas: ___ Formed by accumulation, welding and or cementation of deposits it volcanic ejecta (e.g. tuff, agglomerate, lapilli).
- Su S SEDIMENTARY (UNDIFFERENTIATED). Coarse— to fine-grained materials that exhibit some degree of cementation and were deposited by water, wind, gravity, or evaporation.

Psa. Pm. Ph. Cau. Ls. Py. Par

- S1 Sandstone. Composed predominantly of sand-sized particles.
- \$2 Limestone and Dolomite. Composed predominantly of carbonate material.
- Shale. Composed predominantly of clay- and silt-sized particles (e.g. shale, siltstone, mudstone).
- Evaporites. Sediments deposited from solution as a result of evaporation (e.g. gypsum, anhydrite, halite).
- S5 Clastics. Undifferentiated deposits composed of silt— to boulder—sized material. May be angular to rounded.
- Otz, M METAMORPHIC (UNDIFFERENTIATED). Rocks formed through alteration of igneous or sedimentary rock material by pressure, heat, or chemical changes below the weathered zone (e.g. gneiss, schist, slate, marble, quartzite).
 - C ROCK COMPLEXES. Indicated where no areally predominant (greater than 70 percent) rock type is present.

USEAGE

Modifying letter (r) indicater concentrations of resistant secondary carbonate (caliche), silicious, ferrugirous and or gypsiferous material, e.g. Abir.

A3s A5y - Mixed non-rock units; most areally extensive unit is listed first.

A5y(A5i) - Parenthetic unit underlies thin veneer of overlying mapped unit.

S5to - Established formations may have a supplemental letter added to distinguish formal designation (e.g. Terriary Ogallala Fm.).

EXPLANATION OF GEOLOGIC UNITS

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MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SAMSO

Marie Marie Control of Charles See

TABLE

SIGRO NATIONAL INC.

Information Required for Describing Soils	9	For undisturbed soils add information	on straincation, degree of compactiness, cementation, moisture conditions and drainage characteristics.		Give typical name; indicate approximate procedures of sand and gravel, max, size; angularity, surface cordition, and hardness of the coarse	grains; local or geologic name and other pertinent descriptive information; and symbol in parentheses.	Example: Silv sand, gravelly: about 20% hard.	angular gravel particles 1/2-in, maximum size; rounded and sub-angular sand grains coarse to fine;	dry strength; well compacted and moist in place; alluvial sand; (SM).			Give typical name, indicate degree and character of plasticity, amount and maximum size of coarse grains, color	in wet condition, odor if any, local or geolog:c name, and other pertinent descriptive information; and symbol in narenthese	-	For undisturbed soils and informa- tion on structure, stratification, consistency in undisturbed and re- molded states, moisture and drain	age conditions.	Example: Clayey silt, brown, slightly plastic,	small percentage of fine sand, numerous vertical root holes, firm and dry in place, loess, (ML).
cedures han 3 inches sted weights)		ind substantial particle sizes.	range of sizes missing.	ow plasticity.	procedures see	nd substantial particle sizes.	range of sizes missing.	w plasticity.	procedures see	ures 40 Sieve Size	Toughness (Consistency near PL)	None	Medium	Slight	Slight to medium	чён	Slight to medium	r, spongy feel ture.
Field Identification Procedures (Excluding particles larger than 3 inches and hasing fractions on estimated weights)	\$	lide range in grain sizes and substantial amounts of all intermediate particle sizes.	edominantly one size or a with some intermediate sizes	Nonplastic fines or fines with low (for identification procedures see	fines (for identification procedures relow).	ide range in grain sizes and substantial amounts of all intermediate particle sizes.	redominantly one size or a range of with some intermediate sizes missing.	Nonplastic fines or fines with low plasticity. (for identification procedures see M.L. below)	Plastic fines (for identification procedures see	Identification Procedures on Fraction Smaller than No. 40 Sieve Size	Dilatancy (Reaction to shaking)	Quick to slow	None to very	Slow	Slow to none	None	None to very	Readily identified by color, odor, spongy feel and frequently by forous texture.
Field I (Excluding 1		Wide range in amounts of	Predominantly with some in	Nonplastic fines	Plastic fines (f CL helow).	Wide range in amounts of	Predominantly with some int	Nonplastic fines	Plastic fines (for CL below).	Iden on Fraction S	Dry Strength (Crushing characteristics)	None to si II	Medium to high	Slight to medium	Slight to medium	High to very high	Medium to high	Readily identificand frequently
Typical Names	•	Well-graded gravels, gravel-sand mix- tures, little or no fines.	Poorly-graded gravels, gravel-sand mix- tures, little or no fines.	Silty gravels, gravel-sand-silt mixtures.	Clayey gravels, gravel-sand-clay mix-	Well-graded sands, gravelly sands, little or no fines.	Poorly graded sands, gravelly sands, httle or no fines.	Silty sands, sand-silt mixtures.	Clayey sands, sand-clay mixtures.			Inorganic silts and very fine sands, rock flour, silty or clayey fine sands or clayey silts with slight plasticity.		Organic silts and organic silty clays of low plasticity.	Inorganic silts, micaceous or distoma- ceous fine sandy or silty soils, elastic silts.	Inorganic clays of high plasticity, fat clays.	Organic clays of medium to high plas- ticity, organic silts.	Peat and other highly organic soils.
Group Symbols	ſ	GW	GP	CM	၁၁	SW.	SP	SM	sc			ML	U	10	H W	СН	OH	P
Major Divisions	2	es be	vels islf of c larger i vec size y be use (Clean (chitten n on	Cra than is tion is No. 4 s size ma eve size	More frac	nadi nadi	o to the state of	s. than the since of the since	noM ani		5.691	O bns mil biu nadt	ani2	s .	Al Clay	Liqui		Highly Organic Soils
	-	500	.oV na	d <u>1781</u> 0	ial is la asse.	SICAC	Ο Υίλεα αι ο Yisa αι			i		थ्यः उन्ह	2211	SICYC:	n to tis	d nadi	этоМ.	H

UNIFIED SOIL CLASSIFICATION SYSTEM

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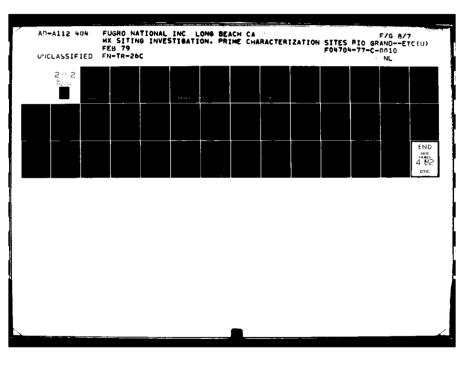
TABLE A-2

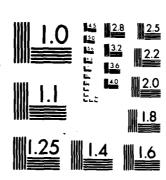
UGRO NATIONAL, INC

APPENDIX B
GEOTECHNICAL DATA - JORNADA DEL MUERTO

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BORING AND TRENCH LOGS	
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LOG OF BORING JM-B-11	Figure B-
LOG OF TRENCH JM-T-2	Figure B-
LOG OF TRENCH JM-T-4	Figure B-
LOG OF TRENCH JM-T-14	Figure B-
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CDAIN CITE CUDVES CRD TESTS	Figure R-



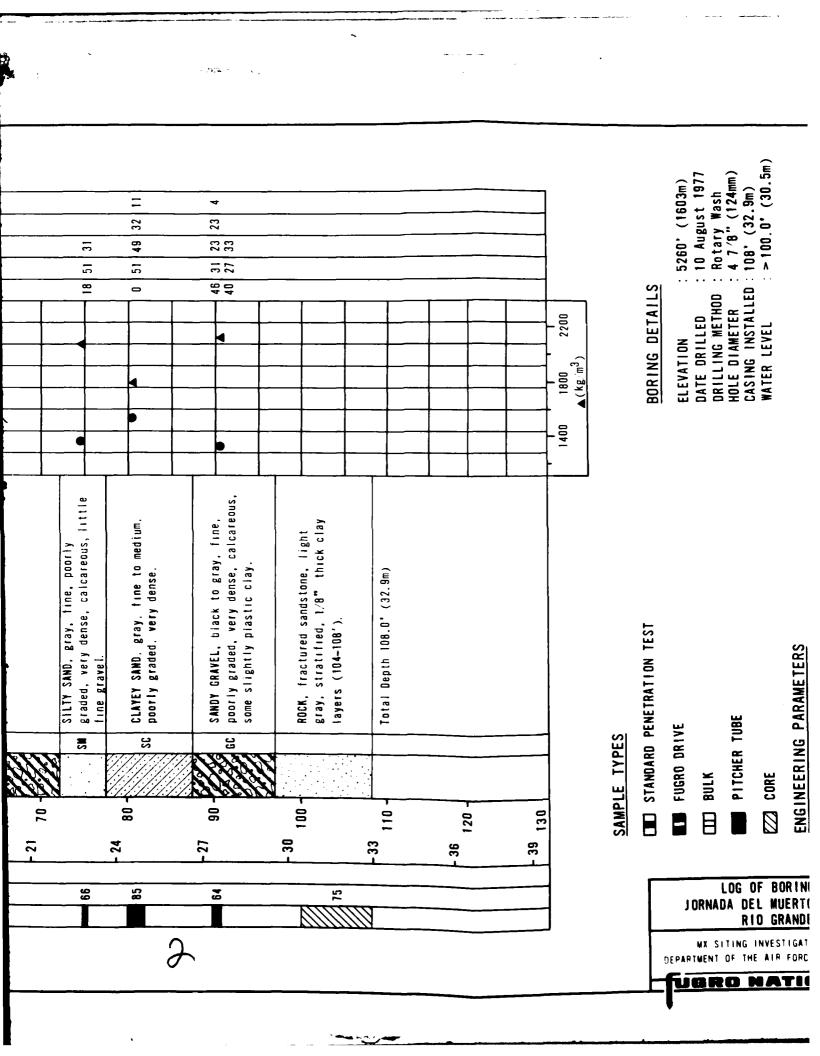


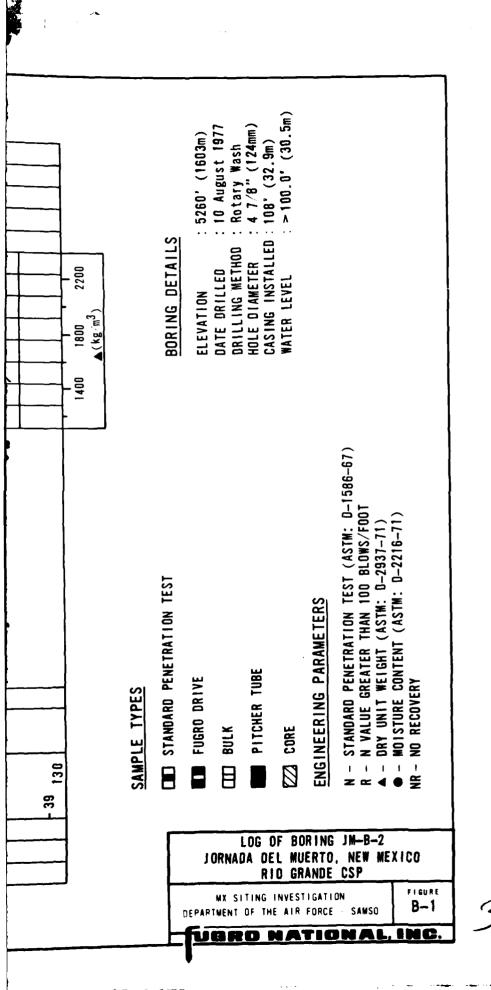
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	SOIL DESCRIPTION	CLAYEY GRAVEL, brown, fine to coarse, poorly graded, loose, angular, little	Sand.	CLAY brown soft (3-18") fire	10-25°, slightly to medium plastic, calcareous.					CLAYEY GRAVEL, black to brown, fine	to coarse, poorly graded, dense, subangular, calcareous, little sand.			
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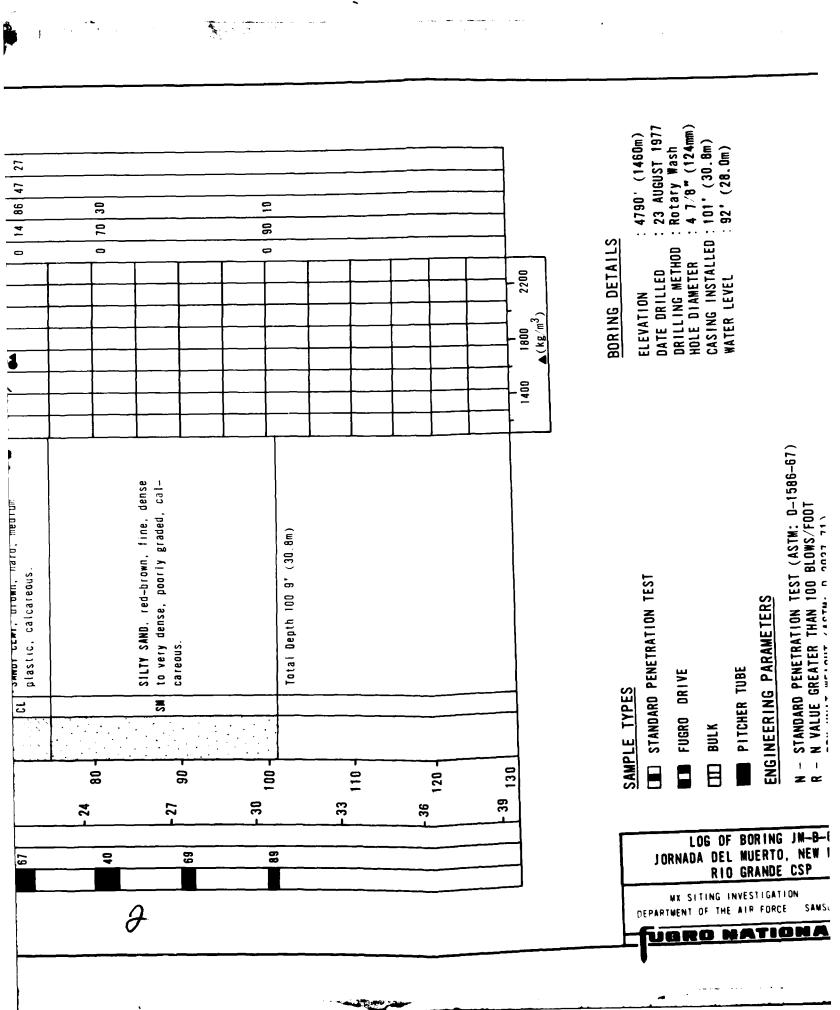


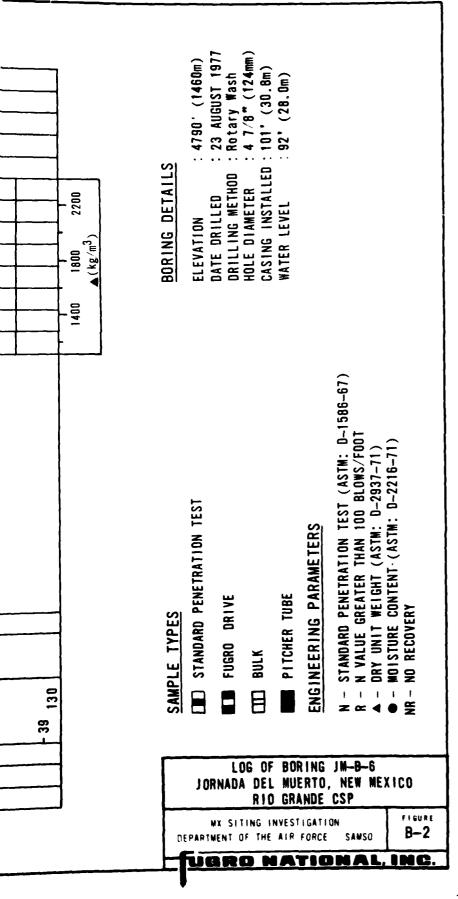


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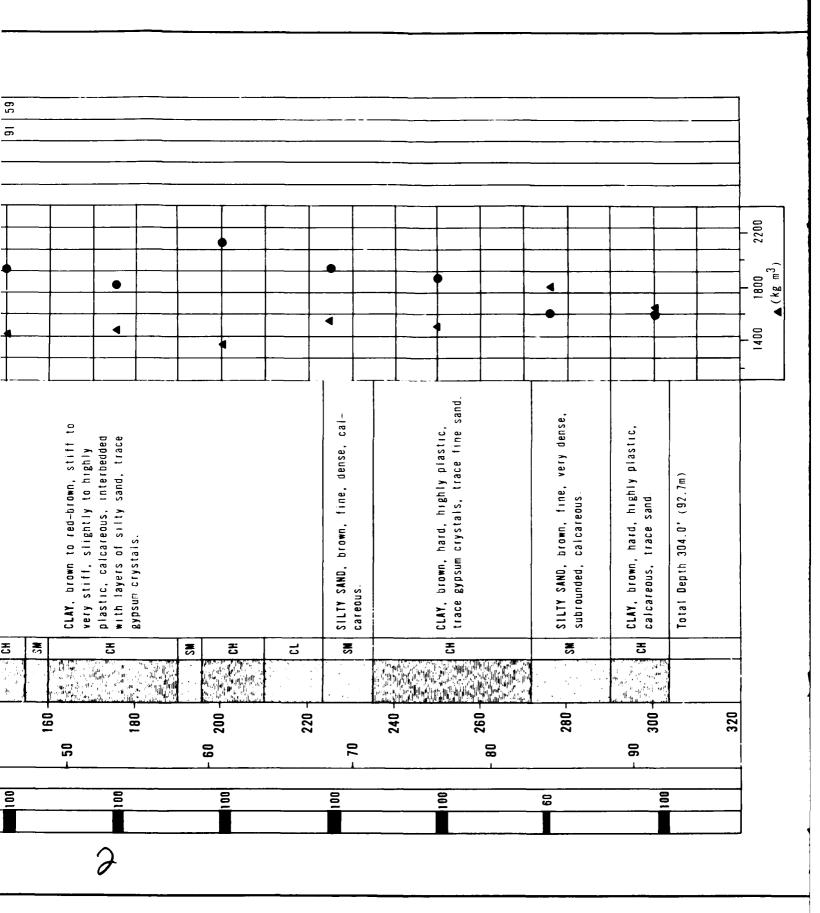
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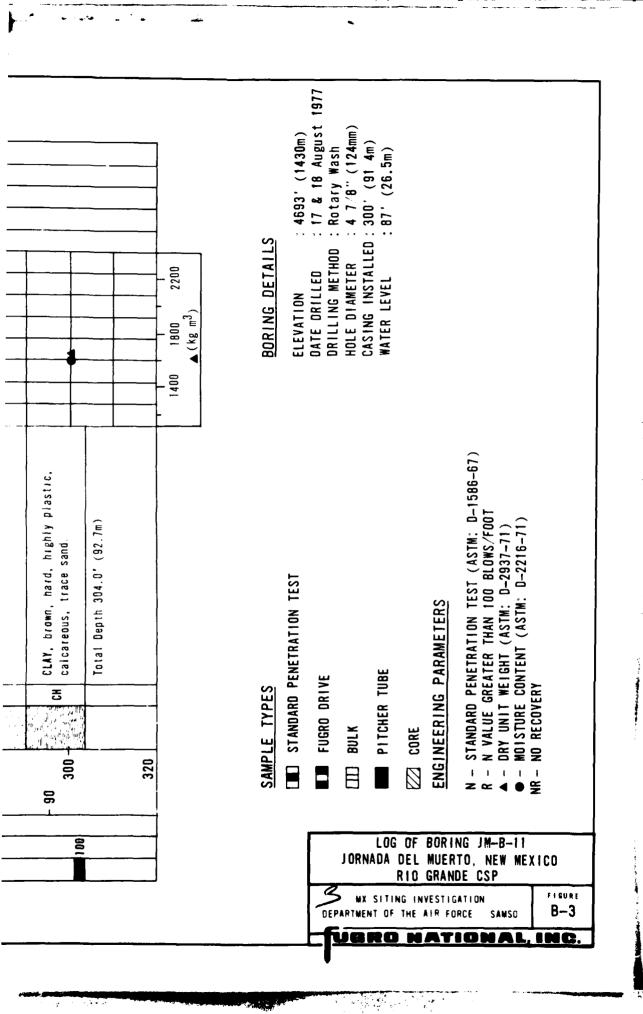
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···	SOIL DESCRIPTION					SAND, brown, fine, poorly	dense, subrounded, trace silt (38°-55°).		CLAYEY SAND, gray to brown, fine to coarse, poorly graded, dense, cal-	of gypsum crystals.	CLAY, gray to brown, stiff, highly plastic, calcareous, lenses of		SILTY SAND, brown, fine, poorly graded, very dense, subrounded, calcareous.			ı	
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BULK SAMPLE	METERS S	TH E	LITHOLOGY	nscs	CONSISTENCY	SOIL DESCRIPTION		ALY:			
BUL	=	FEET	- 1		CON		GR	SA	FI	LL	PI
	- 1	2 -			Soft		4	28	70	25	12
	- 2 - 3	6 -		CL	Stiff	SAMBY CLAY, reddish brown, slightly plastic, calcaraous, trace gravel to 3" (7.6cm), eccasional cobbles to 6" (15.2cm) and boulders to 12" (30.5cm).	10	30	60	23	10
	-4	12-		BC .	Medium dense	SANDY GRAVEL, red-brown, fine to coarse, well graded, subangular to subrounded, calcareous, little clay, stage II caliche layer (15.5-16.5°), cebbles to 6° (15 2cm).		24		21	8
\coprod	1			1							
	-5	16 -		GP	Yery dense	Tetal Depth 18.5' (5.0m)	72	24	4		NF
		18-				Stability of Vertical Walls: Stable					
	-6	20 -									
		22			<u> </u>			_			L

TRENCH DETAILS

SURFACE ELEVATION : 5280° (1603m)

DATE EXCAVATED : 3 August 1977

SURFACE GEOLOGIC UNIT : A1/A5i

TRENCH LENGTH : 50° (15 2m)

TRENCH ORIENTATION : EW

LOG OF TRENCH JM-T-2 JORNADA DEL MUERTO, NEW MEXICO RIO GRANDE CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

FIGURE B-4

BULK SAMPLE	WETERS -	EPTH H	LITHOLOGY	nscs	CONSISTENCY	SOIL DESCRIPTION	1	SIEV IALY:			
BUL	-		5		CON	0012 DE0011110N	GR	SA	FI	LL	PI
	0	0 2 -					0	28	72		NP
	- 2	4 - 6 -		S L	Very stiff	SANDY SILT, white to brown, slightly plastic, catcareous, thin layers of brown, slightly plastic clay with gypsum crystals; stage I caliche (1.5-11.5°).	G	23	77		ΝP
	- 3	10 -									
	-	12-		sc	Dense	CLAYEY SAND, brown, fine to coarse, angular to subangular, trace gravel, gypsum throughout.	7	51	42		NP
	1				Very dense			38	62	34	11
	-5			CL	Stiff	SAMDY CLAY, brown, slightly plactic, gypsum crystals throughout.	,	32	67	33	10
	-6	20 -				Total Depth 18.0° (5.5m) Stability of Vertical Walls: Stable					
		22									

TRENCH DETAILS

SURFACE ELEVATION : 4880° (1428m)
DATE EXCAVATED : 5 August 1977

SURFACE GEOLOGIC UNIT : A5y

TRENCH LENGTH : 50° (15.2m)
TRENCH ORIENTATION : EW

LOG OF TRENCH JM-T-4 JORNADA DEL MUERTO, NEW MEXICO RIO GRANDE CSP

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSC FIGURE B-5

METERS HIGH	1 5	nscs	CONSISTENCY		- 1	SIEV	_	
BULK SAN METERS FEET	1 5]	CONS	SOIL DESCRIPTION	GR	SA	FI	LL P
2		SM	Loose					N
2 8		SM	Medium dense	SILTY SAND, brown, fine to medium, poorly graded, subrounded to subangular, calcareous, stage I caliche (5-10°), trace gravel (10-13°).			19	N
12					10	75	15	N
14		SP- SM	Medium dense	SAND, brown, fine to coarse, poorly graded, subangular to subrounded, calcareous, trace silt (13-17').	2	91	7	N
18	-	SP			2	94	4	N
-6 20				Total Depth 18.5° (5.8m) Stability of Vertical Walls: Unstable 0-5' (0-1.5m) Stable 5-10' (1.5-3.0m) Unstable 10-18.5' (3.0-5.6m)				
20				Unstable 0-5' (0-1.5m) Stable 5-10' (1.5-3.0m)				
SURI Dat Suri	FACE ELEVATION E EXCAVATED FACE GEOLOGIC VCH LENGTH		: 2 Aug	(1447m) LOG OF TRENCH ust 1977 JORNADA DEL MUERTI RIO GRANDE), !	IEW		XIC

	^								PERCE	IT FIN	ER BY 1	WEIGHT				
<u> </u>	E :R (a)	SAMPLE I	NTERVAL		S	TANDARI	SIEV						DARD S	SIEVE	10	PAR SIZI
BOR ING Number	SAMPLE Number			BLDRS.	COBE	LES		GRA	VEL			AZ	ND		SIL	T OR
8 3	SAI	FEET	METERS	24"	12"	6"	3"	1½"	3/4"	3/8"	4	10	40	100	200	.005
JM-B-11	B-1A	0.0-2.0	0.00-0.61									100	99	97	95	
	P1	5.5-6.2	1.68-1.89													
	P-2	10.5-11.2	3.20-3.41											1	T	
	P3	15.5-16.2	4.72-4.94										l			
	P-4	20.7-21.4	6.31-6.52													
	B-5	25.5-26.5	7.77-8.08					100	85	76	67	60	46	27	21	
	P-6	28.0-28.7	8.53-8.75									1	1	T		
	P-7	31.0-31.7	9.45-9.66		<u> </u>										I	
	P-8	40.2-40.9	12.25-12.47									100	97	43	7	
	P-9	50.5-51.5	15.39-15.70											t		
	P-10	61.0-61.8	18.59-18.84									100	80	3	3	
	P-11	71.1-71.8	21.67-21.88						100	96	83	66	54	50	48	3
	P-12	80.5-81.2	24.54-24.75		Ī		Γ			T				T	T	
	P-13	90.5-91.2	27.58-27.80			<u> </u>				l	<u> </u>	<u> </u>		1	f	
	P-14	100.5-101.2	30.63-30.85			<u> </u>	<u> </u>					†	†	†	1	
	P-15	126.3-127.0	38.50-38.71	1		 				 		†	t —	t —	1	
			45.87-46.09	t —	<u> </u>	<u> </u>	t					†	-	†	T	-
	F-17	175.5-176.2	53.49-53.71			 		<u> </u>	 	<u> </u>	 	1		 	t^{-}	
	P-18	200.5-201.2	61.11-61.33		<u> </u>	<u> </u>	t	<u> </u>		<u> </u>		 	<u> </u>	†	1	 -
			68.73-68.95				<u> </u>			t	 		<u> </u>			
	P-20	250.5-251.2	76.35-76.57							 	 	 			$\overline{}$	<u> </u>
	P-21	275.4-276.0		1 1		l		-		- · -		† •		 	†	ţ
	P-22	302.0-302.7	92.05-92.26				<u> </u>			\vdash		\leftarrow	 	1	 	
		302.0 302.1	-2.00 52.20	ti		 	 	<u> </u>	-			 	 -	 	 	
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NOTES:

(a) Sample types

- (c) USCS Unified Soil Classification System
- SS Standard split spoon
- P Pitcher
- D Fugro Orive
- B Bulk
- (b) MP Not Plastic

 Indicates that test has been performed and results are included in this report.

						TERRE	'DC				I_S I TU			C	OMPACTE		4.5		요중		8
ARD S	IEVE N	10	PART	(ICLE	1	TERBE NITS		USCS	DRY	UNIT	MOISTURE Content (%)	SATURATION (%)		MAXI	MUM	OPTIMUM Moisture (%)	SPECIFIC GRAVITY OF SOLIDS	TRIAXIAL	UNCONFINED COMPRESSION	<u></u>	CONSOLIDATION
p		SIL	T OR C		l '''	-110	\ U /	(c)	WEI	GHT	IIST INTE (%)	TURA (%)	VOID RATIO	DRY DE	HSITY	TIN (%)	SA	IAX	E PR	DIRECT Shear	1801
40	100	200	.005	.001	LL	PL	PI		(pcf)	(kg/m³)	9 0 2	SA	S &	(pcf)	(kg/m ³)	0 =	8 8 8	TR	5 5	3	흜
99	97	95						ML													
								ML	101.3	1623	13.2	54	.66								
					23	8	15	CL	113.4	1817	11.0	61	.49						*		
								CL	108.9	1745	16.4	81	.55								
			L	 	ļ	ļ		SM	108.1	1732	13.6	66	.56		ļ	Ļ				*	
46	27	21		↓	ļ	ļ	L	SM		ļ					<u> </u>	L				└	—
L			ļ	.	28	10	18	CL	105.1	1684	15.6	70	.60		ļ				L	├ ──┤	*
<u> </u>			 _	 	56	27	29	CH	112.3	1799	13.5	73	.50	<u> </u>	ļ				*	┟──┤	
27	43	7	ļ	ļ	 	 	<u> </u>	SP-SM	108.0	1730	8.8	42	.56	ļ	<u> </u>				ļ	┝─┤	
	<u> </u>	<u> </u>	ļ	ļ	 		<u> </u>	SP-SM	100.3	1607	22.7	90	.68	ļ	<u> </u>		 		├	 	
n0	3	3 48	-	-,	50	21	20	SP	107.0 99.7	1714	18.8	88 77	.57	-	 	 	 			┟──┤	
	50	40	3	3	50	21	29	SC SC	116.4	1597 1865	15.0	91	.45		 	 	1		 		
 		\vdash		 	 -	 		CH	81.8	1310	37.3	95	1.06		 	 	 	<u> </u>	 		
			· · · · · ·	†	-	<u> </u>	 	CH CH	84.9	1360	34.3	94	.99		 	 	†		 		
<u> </u>				 	-	\vdash		CH	103.5	1658	19.4	83	.63				 		 		
				†	91	32	59	CH	98.6	1580	15.4	59	71		<u> </u>	 	†		*		
				†	 			CH	92.8	1487	21.8	72	.82		 	 	 		1		
				t				СН	85.5	1370	32.4	91	.97			<u> </u>	1				
								SM	97.2	1557	25.7	95	.73						Γ		
								СН	94.7	1517	23.3	81	.78				I	L	I		
								SM	111.9	1793	15.8	84	.51			I	<u> </u>	<u> </u>		<u> </u>	<u> </u>
								CH	102.8	1647	15.3	65	.64			I	<u></u>		L		
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SUMMARY OF LABORATI BORING JI JORNADA DEL MUERTO, NEW I

MX SITING INVESTIG DEPARTMENT OF THE AIR FO

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	1	11	UT I 2-I			C	OMPACTE	0			_ =		3		
202U (c)	DRY U	GHT	MOISTURE Content (%)	SATURATION (%)	VOID RATIO	MAX I Dry de	MUM	OPTIMUM Moisture (%)	SPECIFIC GRAVITY OF SOLIDS	TRIAXIAL	UNCONFINED COMPRESSION	DIRECT SHEAR	CONSOLIDATION	CHEMICAL	RELATIVE Dens; ty
	(pcf)	(kg/m³)	≅ ວ	S	22	(pcf)	(kg/m³)	5 =	2 2 2	=	50	ᅙᅘ	5	3	2 5
ML.															
ML	101.3	1623	13.2	54	.66										
CL	113.4	1817	11.0	61	.49						*				
CL	108.9	1745	16.4	81	.55										
SM	108.1	1732	13.6	66	.56							*			L
SM															
CL	105.1	1684	15.6	70	.60		-						*		
СН	112.3	1799	13.5	73	.50				L		*				
SP-SM	108.0	1730	8.8	42	.56			L			.				\sqcup
SP-SM	100.3	1607	22.7	90	.68			ļ			ļ				
SP SC	99.7	1714 1597	18.8	88 7 7	.57		<u> </u>				├				├ ──
SC	116.4	1865	15.0	91	.45						*	├─┤			\vdash
CH	81.8	1310	37.3	95	1.06			-	<u> </u>		 				
CH CH	84.9	1360	34.3	93	.99		ļ	ł	 -			\vdash			⊢ ⊸d
CH	103.5	1658	19.4	83	.63		·	ļ. —			├ ─	-			$\vdash \vdash \vdash$
CH	98.6	1580	15.4	59	71						*	-			\vdash
CH	92.8	1487	21.8	72	.82			 			 "				- -
CH	85.5	1370	32.4	91	.97			 			 	-			1
SM	97.2	1557	25.7	95	.73					-	-				
СН	94.7	1517	23.3	81	.78			_			† —				
SM	111.9	17 93	15.8	84	.51		<u> </u>		f		1 —				
CH	102.8	1647	15.3	65	.64		<u> </u>		 						
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SUMMARY OF LABORATORY TEST RESULTS
BORING JM-8-11

JORNADA DEL MUERTO, NEW MEXICO, RIO GRANDE CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SAMSO

B-1

UGRO NATIONAL, INC.

THE RESERVE THE PROPERTY OF THE PARTY OF THE

2	SAMPLE	SAMPLE INTERVAL	NTERVAL	TIOS	COMP. S.	UNCONFINED MP. STRENGTH	DRY DE	DENSITY	CONTENT	DEGREE OF	HEIGHT
	×0.	FEET	METERS	TYPE	ks f	kN /m2) od	kg/m³	(%)	(%)	DIAMETER
1-8-11	P-3	14.0-14.8	4.3-4.5	10	2.2	105	93.3	1497	16.0	53.7	2.40
	P-11	80.0-80.8	24.4-24.6	CL	2.4	116	112.7	1809	13.8	75.2	2.40
	P-13	100.8-101.6	30.7~31.0	¥	2.0	97	110.9	1780	15.8	81.1	2.40
1M-B-2	P-1	5.0-5.8	1.5-1.8	13	2.3	111	106.9	1718	12.8	60.2	2.40
	P-4	20.0-20.8	6.1-6.3	כר	0.4	20	96.2	1544	24.3	87.4	2.00
	88	80.0-80.8	24.4-24.6	10	2.4	115	117.0	8781	14.5	89.0	2.40
14-8-3	P-1	5.0-6.0	1.5-1.8	ו	1.1	51	102.6	1647	19.3	81.2	2.40
	5.	25.0-25.9	7.6-7.9	13	4.4	211	114.8	1843	11.1	64.0	2.09
1M-8-4	<u>-</u>	5.8-6.4	1.8-2.0	13	4.9	235	104.2	1672	10.7	47.0	2.09
	P3	15.0-15.8	4.6-4.8	70	2.9	138	109.8	1762	14.1	71.0	2.09
	F-7	50.0-50.8	15.2-15.5	ΗS	4.0	190	88.3	1417	31.2	92.8	2.09
	P-10	80.0-80.8	24.4-24.6	CL	1.7	80	92.3	1481	27.2	89.1	2.09
JM-8-5	P-1	5.0-5.9	8.1-2.1	13	1.5	11	79.5	1276	20.4	49.3	2.09
JM-8-6	7	21.1-21.9	6.4-6.7	SC	3.4	160	117.2	1881	6.8	41.8	1.74
	P-10	70.0-70.8	21.3-21.6	10	8.0	385	97.0	1557	25.2	92.1	2.40
H-B-7	5-2	20.5-21.0	6.2-6.4	13	16.0	766	113.3	1818	15,1	84.0	2.00
JM-8-8	P-10	70.0-70.8	21.3-21.6	3	11.0	528	117.9	1892	9.4	59.1	2.40
JM-8-9	P-5	25.8-26.5	7.9-8.1	ಶ	2.3	108	106.8	1714	14.3	66.9	2.40
	2	74.8-75.5	22.8-23.0	5	7.3	350	99.0	1589	22.3	85.7	2.40
18-8-10	P-7	40.0-40.7	12.2-12.4	5	3.2	155	103.2	1658	16.0	68.4	2.40
	P-15	147.5-148.2	45.0-45.2	3	16.4	787	96.9	1555	24.0	87.6	2.40
	P-18	225.0-225.7	68.6-68.8	CL	10.8	517	104.2	1672	18.1	83.7	2.40
18-B-11	P-2	10.5-11.2	3.2-3.4	ಬ	2.8	132	113.4	1820	11.0	61.4	2.40
	7	31.0-31.7	9.4-9.7	73	3.5	167	112.3	1802	13.5	72.8	2.40
	=	71.1-71.8	21.7-21.9	æ	2.7	129	89.7	1600	19.7	11.1	2.40
	P-16	150.5-151.2	45.9-46.1	НЭ	9.4	452	98.6	1583	15.4	58.6	2.40
JM-8-12	무	70.0-10.1	21.3-21.5	ដ	4.6	219	109.5	1757	16.3	81.8	2.40
1M-8-14	87	50.0-50.8	15.2-15.5	ย	7.1	342	99.5	1597	22.0	85.6	2.40
18-8-15	P-14	150.0-150.9	45.7-48.0	M.	4.0	193	110.2	1769	10.0	50.9	2.40

SUMMARY OF UNCONFINED COMPRESSION TEST RESULTS JORNADA DEL MUERTO, NEW MEXICO, RIO GRANDE CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

TABLE B-2

BACK PRESSURE	kN/m ²	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0			
PRES	ksf	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0			
STRAIN	\simeq	0.03	0.03	0.03	0.8	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1			
MAXINUM DEVIATOR FRESS(O1-O3)	kN/m²	517	800	1447	1044	259	565	469	249	1001	738	891	999	2299	580	828			
1 74		10.8	16.7	30.2	21.8	5.4	11.8	9.8	5.2	20.9	15.4	18.6	13.9	34.1	12.1	17.3			
NING RE(σ_3)	км/m2	240	378	584	378	48	240	240	48	288	144	378	115	412	378	723			
PRESSURE (03)	ksí	5.0	7.9	12.2	7.9	1.0	5.0	5.0	1.0	0.0	3.0	7.9	2.4	8.6	7.9	12.1			
CONTENT		14.6	14.6	14.6	7.8	11.6	13.7	13.7	5.7	6.5	11.2	10.5	8.9	9.6	20.3	14.7			
DENSITY	kg/m ³	1568	1568	1568	1618	1735	1685	1599	1759	1721	1946	1970	1674	1934	1681	1812			
ORY DE	pc t	17.78	97.7	7.76	100.8	108.1	105.0	93.6	109.6	187.2	121.2	122.7	104.3	120.5	104.7	112.9			
TY PE SF	TEST	C)	as	යා	nn n	D.S	03	ຄວ	ao	03	ຄວ	ຄວ	go	93	8	00			
2011	TYPE	13	CL	เร	SH	CL	כר	13	SP	dS	73	73	N.S.	HS.	ಚ	13			
INTERVAL	METERS	15.2-15.5	15.2-15.5	15.2-15.5	15.5-15.7	3.0-3.3	4.6-4.8	4.8-5.1	4.6-4.8	4.8-5.1	8.5-8.7	8.7-8.9	7.6-7.9	7.9-8.1	24.6-24.8	24.8-25.1			
SAMPLE	FEET	50.0-20.8	50.0-20.9	50.0-20.8	50.9-51.4	10.01-10.8	15.0-15.8	15.8-16.8	15.0-15.8	15.8-16.6	27.8-28.6	28.6-29.3	25.0-25.8	25.8-26.8	80.8-81.5	81.5-82.5			
SAMPLE	<u>.</u>	P-8	P-8	P-8	P-8	P-2	P-3	F.3	P-3	F-3	9-6	P-6	P-5	P-5	P-12	P-12			
9	. 08	JM-8-1*				JM-8-3			JM-8-6		JM-8-7		1M-8-8		111-8-17				

Multi-stage test

SUMMARY OF TRIAXIAL SHEAR TEST RESULTS JORNADA DEL MUERTO, NEW MEXICO RIO GRANDE CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

TABLE B-3

BORING	SAMPLE	SAMPLE I	NTERVAL	SOIL	NORMAL	STRESS	MAXI SHEAR S	MUM Trength
NO.	NO.	FEET	METERS	TYPE	ksf	kN/m²	ksf	kN/m 2
JM-B-2	P-3	15.0-15.8	4.57-4.82	CL	6.0	290	3.7	177
	P-3	15.0-15.8	4.57-4.82	CI	1.0	48	1.2	56
J M- B-5	P-5	32.3-33.0	9.85-10.06	SC	8.0	386	5.1	246
	P-5	32.3-33.0	9.85–10.08	SC	3.0	145	2.5	118
	P-9	73.0-73.7	22.25-22.46	ML	10.9	524	1.1	368
	P-9	73.0-73.7	22.25-22.46	ML	7.1	338	4.8	228
JM-8-6	P-8	50.0-50.8	15.2-15.5	SM	10.0	479	6.5	312
	P-8	50.0-50.8	15.2-15.5	SM	5.0	241	4.0	191
JM-B-7	P-7	40.0-40.5	12.2-12.3	M2	12.2	586	11.4	548
	P-7	40.0-40.5	12.2-12.3	SM	4.0	193	7.1	339
JM-8-8	P-3	15.0-15.5	4.6-4.7	MZ	7.9	379	5.4	261
	P-3	15.0-15.5	4.6-4.7	MZ	1.0	48	0.7	34
JM-B-9	P-1	5.0-5.8	1.5-1.8	ML	6.5	310	5.0	241
	P-1	5.0-5.8	1.5-1.8	ML	1.0	48	1.3	61
JM-B-10	P-1	5.0-5.7	1.5-1.7	ML	6.5	310	5.4	261
	P-1	5.0-5.7	1.5-1.7	ML	i.0	48	2.2	105
	P-4	20.0-20.7	6.1-6.3	SM	7.2	345	4.8	228
	P-4	20.0-20.7	6.1-6.3	SM	2.2	103	1.8	872
JM-8-11	P-4	20.7-21.4	6.3-6.5	ML	5.8	276	6.3	302
	P-4	20.7-21.4	6.3-6.5	ML	2.0	97	3.4	165
JM-B-12	P-5	25.0-25.7	7.6-7.8	SP-SM	7.9	379	5.8	275
	P- 5	25.0-25.7	7.6-7.8	SP-SM	2.2	103	1.7	81
JM-B-13	P-1	5.0-5.7	1.5-1.7	SC	5.8	276	4.5	217
	P-1	5.0-5.7	1.5-1.7	SC	1.0	48	1.3	632
JM-8-14	P-1	5.0-5.7	1.5-1.7	SM	5.8	276	4.0	193
	P-1	5.0-5.7	1.5-1.7	MZ	1.0	48	1.0	48
JM-8-15	P-3	17.0-17.7	5.2-5.4	SP-SM	7.9	. 379	5.4	260
	P-3	17.0-17.7	5.2-5.4	SP-SM	2.2	103	1.6	335
JM-8-17	P-1	5.0-5.7	1.5-1.7	ML	5.8	276	4.6	221
	P-1	5.0-5.7	1.5-1.7	ML	1.0	48	2.2	104

SUMMARY OF DIRECT SHEAR TEST RESULTS JORNADA DEL MUERTO, NEW MEXICO RIO GRANDE CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

B-4

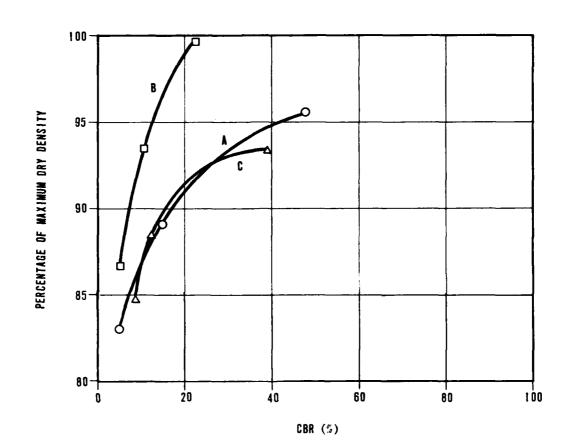
	1TY (%)	43.7	17.5	4.9		22.3	11.0	5.3		39.1	12.7	8.6				
MAXIMUM NAXIMUM	5	92.6	89. 1	83.1		93.6	93.5	86.7		93.3	88.6	84.8				
COMPACTED	(%)	5.0	4.7	4.7		8.2	7.8	7.4		7.2	6.5	7.6				
COMPACTED DRY DENSITY	kg/m3	2074	1933	1804		1930	1812	1680		1873	1778	1701				
	pcf	129.5	120.7	112.8		120.5	113.1	104.9		116.9	111.0	106.2				
OPT I MUN MOISTURE	(%)			9.0	_			9.5				3.				
MAXIMUM Dry density	kg/m3			1712				1938				2007				
	pc f			135.5				121.0				125.3				
SPECIFIC	GKAVIIT			2.1				2.8				2.65	-			
ATTERBERG Limits	<u>-</u>			9			•	* *				*				
ATTE	11			24												
PERCENT PASSING	#200			8				34				7				
1108	ווג			SC-SM				ES.				ES.				
COMPOSITE	NUMBER			~				40				ပ				

P NOT PLASTIC

CALIFORNIA BEARING RATIO (CBR) TEST RESULTS JORNADA DEL MUERTO, NEW MEXICO, RIO GRANDE CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

B-5



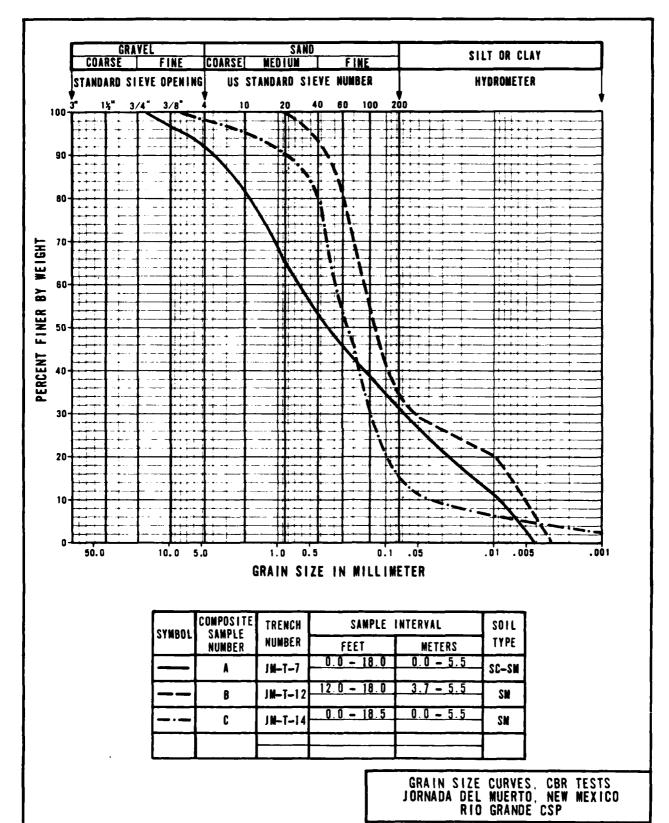
SYMBOL	COMPOSITE Sample Number	SOIL TYPE
0	A	SC-SM
	В	SM
Δ	C	SM
		_

CALIFORNIA BEARING RATIO
(CBR) CURVES

JORNADA DEL MUERTO, NEW MEXICO, RIO GRANDE CSP

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE S

B-7



FIGURE

B-8

SAMSO

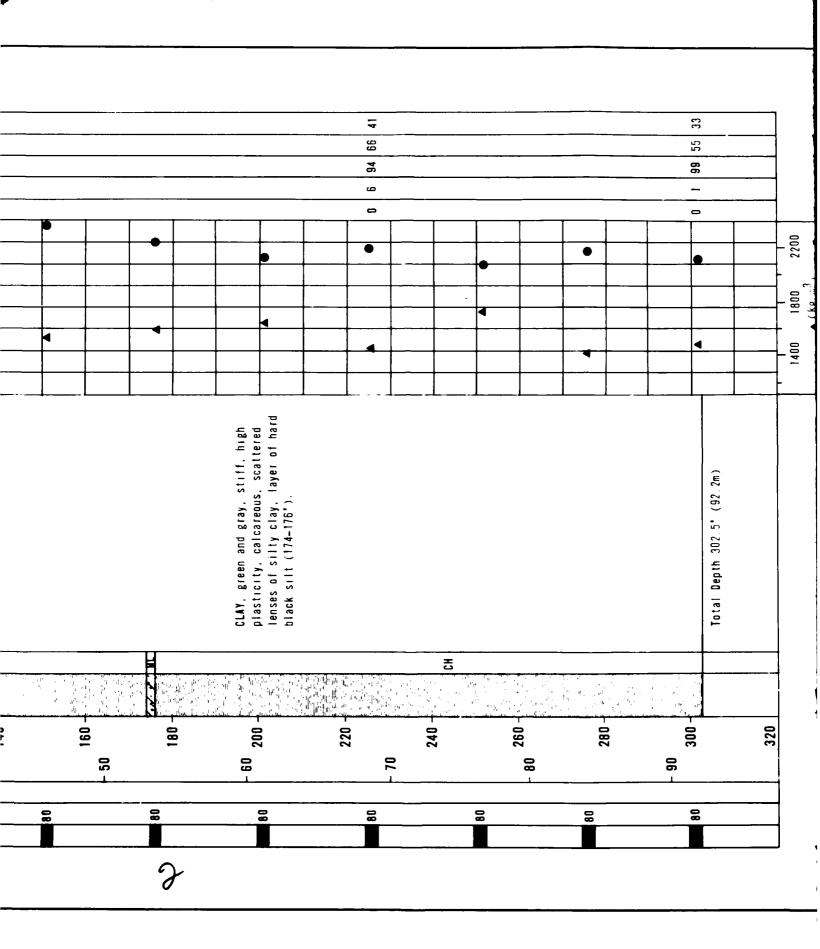
MX SITING INVESTIGATION

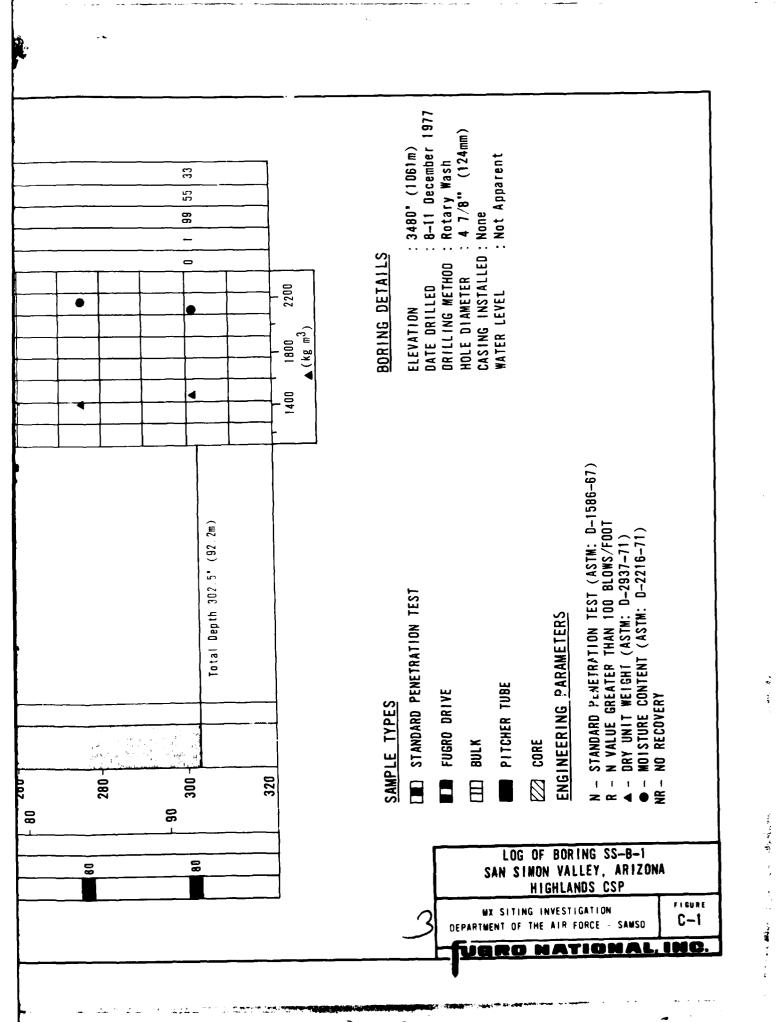
DEPARTMENT OF THE AIR FORCE

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SIEVE	SAFI		43		<u> </u>	- 99								<u>ස</u> ෆ								8				_
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▲(pcf) 100 110 120 130 140	+22 ~	 	1			+		+		\dagger		\dagger			寸				I^-	+			\dashv		 	_
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80	+5	•											-	4						\top		•	9			_
	SOIL DESCRIPTION	coarse, poorly graded, dense, angular	silt, a little fine gravel.	SANDY GRAVEL, light brown, fine, we graded medium dense to dense sub-	angular to subrounded, calcareous,	with line to coarse gravel, trace of	CLAYEY SAND, light red brown, fine to	medium, poorly graded, dense, angular () to subrounded, calcareous, some low	plasticity clay.	SILTY CLAY, green and red brown,	medium to high plasticity, calcareous, trace of fine sand.	CLAY, green, stiff to very stiff,	medium plasticity, calcareous, trace	41.5°), layers of fine to medium	very dense (41.5-44").	SILTY CLAY, gray green, stiff, medium plasticity, calcareous, trace of fine	sand.									
cs	sn	ᇙ	3	SE	3		2	7		2	I									5	5					_
190701	1111	000	0,0											ng 19	914 (4.		ar ag		E. The second	41 1	i		
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7074	ΛN																									_





MPLE TYPE RECOVERY	VALUE	DEP S	TH	LITHOLOGY	ş		ŀ.			A (p		130	140		IEV			
SAMPLE TYPE * RECOVERY	N VA	METERS	FEET	LITHO	nscs	SOIL DESCRIPTION	\vdash	-	-	-	25	30	+		SA	-	LL F	<u> </u>
01		0	0		SM	SILTY SAND, light brown, fine, well graded, loose (0-2'), medium dense (2'-4.5'), calcareous, some non plastic silt.	•		•					3	72	25		
1 04		- 3	10 -		ML	trace of fine gravel. SANDY SILT, brown, firm, non plastic, calcareous; with fine to			•									
1 01						medium sand; scattered zones with a trace of fine gravel.	•							0	47	53		
1 01		- 6		/•/• /	SM	SILTY SAND, brown, fine to medium, medium dense, subangular to sub-rounded, calcareous, some low												
1 0		- 0	20 -	///	ML	plasticity silt and clay; trace of fine gravel. SANDY SILT, brown, firm, non- plastic, calcarsous; some fine	-							0	21	78	•	(P
1 01		- 9		• • • •	SP- SM	sand. SAND, brown, fine to medium, dense subangular to subrounded, cal- careous, trace of non plastic silt	ı			^								
1 01		•	30 -		GP-	trace of fine gravel. SANDY GRAVEL-GRAVELLY SAND, brown, fine to coarse, medium dense to								50	48	2		
		- 12		///	_	dense, subangular to subrounded, calcarseus, with fine to medium sand, trace of silt.												
100		•	40 -		ML	CLAYEY SILT, brown, stiff, low plasticity, calcareous, trace of fine sand, layer of brown, hard,												
		- 15			CL	medium plasticity clay (47.5"- 50") lense of very dense, silty sand (50"-50.5").												
1 01			50 -	1. L.L	MC	Total Depth 51.0' (15.5m)		-										
		- 18	60															
							Ľ	140	0	18 (kg	00 /m ³)		00					
	TAN	DARD O DR		TRATION	TES	Ţ	ELE DAT DRI HOL CAS	VAT E D LLI E D ING	ION RILL NG I IAME	METH TER STAL	00 : LED :	332 12 Hol 6 5 Non	Dece low /8"	Ster (1)	r 19 m Au 68ma	iger		
ENGINE		HER 1		ETERS			WAT		LEVI	_		Not						
N — R —	STAN N V/ DRY	DARB LUE UNIT	PENE GREAT WEIG	TRATION TER THAN THT (ASTI	100	ST (ASTM: 0-1588-67) D BLOWS.FOOT 1-2937-71)				IMO	N V	OR III ALL LAND	EΫ,	AF	RIZ	-		-
NR —				ERI (AS	ı wi :	0-2216-71)	M	t Si	TIN	G 11	EVES	TIGA	TION			T	C-	

TYPE	RECOVERY	VALUE	DEP	HT	, 10 G	ی		┢				pcf)				1	SIEV	E	1	
SAMPLE	% RECO	N VA	METERS	FEET	LITHOLOGY	nscs	SOIL DESCRIPTION	-	5	+-	15	10 1	\leftarrow	-	+	_	SA	1	LL	P
S	70		0	0		GC- GM	SANDY GRAVEL, red brown, fine to coarse, poorly graded, dense to very dense, subangular to sub- rounded, calcareous, some medium to coarse sand, some low plasticity clay and silt.					(%)					33		\vdash	-
	60		- 3	10 -		sc	GRAVELLY SAND, red brown, fine to coarse, poorly graded, very dense subangular to subrounded, calcareous, some fine to coarse gravisme low plasticity clay, scatter	· -	+,	-			•	_	-				! 	
	1 00		- 6	20 -		GC GP	cobbies. SANDY GRAVEL, dark yellow brown, fine to coarse, poorly graded, vedense, subangular to subrounded calcareous, some fine to medium sand, a little low plasticity cla	- '* -		-										
			- 9				SANDY GRAVEL, dark red brown, fir to cearse, poorly graded, very dense, calcareous, a little fine to cearse sand, trace of low plasticity silt. CLAYEY SAND, red and white, fine	}		•	-	<u> </u> ,		-		13	44	43		
			- 12	30 - 40 -		sc	CLAYEY SAND, red and white, fine medium, poorly graded, very dense subangular to subrounded, calcareous; with low plasticity clay a little fine gravel, stage I to stage II caliche. GRAVELLY SAND, red brown and white	· · -	•											
	20			40			fine to coarse, poorly graded, ve dense, subangular to subrounded, calcareous, some fine gravel, som low plasticity clay, scattered caliche nodules.	1												
	80		- 15	50 -			CLAYEY SAND, yellow red, fine to medium, well graded, very dense, subangular to subrounded, calcareous, with low plasticity clay trace of fine gravel. Total Depth 54.0° (16.5m)	<u> </u> -	+	•		<u> </u>				2	52	46	35	12
			- 18	60				╽,		L	L		Ļ	Ĺ				_		
SAMP	LE	ŢŸ	PES								<u> </u>	8 0 0 E/m		22	00					
	S F	TAN UGR ULK	DARD O DR	IVE	TRATION	TES	τ	E L DA DR HO CA		TION DRIL ING DIAN	LED MET IETE STA	HOD R Lle	: 1 : R : 4	3 (lota 7 /	D' (Dece ary /8" a App	wbe Was! (12	r 19 h 4mm			
N — R —	- s	TAN V V/	IDARD ALUE UN I T	PENI GREA WEI	TER THAN GHT (AST	100 M: 8	T (ASTM: D-1586-87) BLOWS/FOOT -2937-71) 0-2218-71)		SA		IM	ON	VA	LLI	IG S EY,	AF			1	-
			RECOV		J (110				-				-	-	I ON			T		eu (

BULK SAMPLE	METERS 3		THOLOGY	uscs	CONSISTENCY	SDIL DESCRIPTION	AN	_	SIS		
	0	0	SIGILY.	-		SANDY GRAVEL, brown, fine to coarse, poorly	T		FI	 	P
Щ				GC	Loose	graded, subangular to subrounded; dry, non- stratified, non cemented, a little cebbles and boulders, maximum size 1.0°, some fine to coarse sand, some low plasticity clay and silt,	41	31	28		
	- 1	4 - 6 - 8 -		GW	Very dense	stage I to stage II caliche. SANDY GRAVEL, gray, fine to coarse, well graded, subangular to subrounded, calcareous, dry, non stratified, moderately to strongly comented stage II to stage III caliche, some cobbles and boulders, maximum size 1.2°, with fine to coarse sand, trace of silt.	49	40	11		
	- 3	10-		CL-	Very stiff	SILTY CLAY-CLAYEY SILT, light brown, low to medium plasticity, calcareous, dry, homogeneous, non cemented, a little fine to coarse sand, trace of fine gravel, scattered hard clay nodules.	5	17	78	44	17
	-4	12-				Total Depth 11.5" (3.5m) Stability of Vertical Walls: Stable					
		14 -									
	-5	16 -									
		18-									
	-6	20 -									
		22									

TRENCH DETAILS

SURFACE ELEVATION : 3400' (1038m)
DATE EXCAVATED : 10 December 1977

SURFACE GEOLOGIC UNIT : A51

TRENCH LENGTH : 29' (8.8m)

TRENCH ORIENTATION : NS

LOG OF TRENCH SS-T-1 SAN SIMON VALLEY, ARIZONA HIGHLANDS CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

C-4

BULK SAMPLE	METERS	PTH ⊷	1 THOLOGY	uscs	CONSISTENCY	9011	DESCRIPTION	1	SIEV			
BUL!	WE T	FEET	=		CONS	2015	DE2041F110N	GR	SA	FI	ıı	PI
	0	0		MZ	Leose	graded, subangular,	rown, fine to medium, well calcareous, dry, non ented, some low plasticity e of fine gravel.	Ti	67	32		
\prod	- 1	2 -		CH	Very stiff	city, calcareous, d	rown, medium to high plasti- ry, homogeneous, weakly ented, some fine sand.	0	25	75	57	37
	- 2	4 -		CL	Hard	dry, homogeneous, m	ow plasticity, calcareous, oderately to strongly to medium sand, stage II e, trace of gravel.	6	38	56		
	- 3	8 - 10 -		sc	Dense		fine to coarse, well graded, ar, with low plasticity clay gravel.	1	58	41		
	-4	12 -	17.77.77.7			Total Depth 12.0° (Stability of Vertic Stable	al Walls;					
	-5	16 -										
		18 -										
	-6	20 -										
		22 TDFM	CH DETAILS					<u></u>				
		SURFA Date Surfa	CE ELEVATION EXCAVATED ICE GEOLOGIC THE LENGTH		: 11 00	(1079m) scember 1977	LOG OF TRENCH SAN SIMON VALLEY HIGHLANDS	1, 1	ARI		IA	

BULK SAMPLE	METERS S	FEET H	LITHOLOGY	USCS	CONSISTENCY	SOIL DESCRIPTION		SIEV ALY:			
<u>a</u>	1		5	<u>_</u> _'	8		GR	SA	FI	LL	P
	0	. 2 ~		SC- SM	Med i um	CLAYEY SAND—SILTY SAND, light brown, fine, poorly graded, calcareous, dry (0-0.5°), slightly moist (0.5° to 3.0°), non stratified, non cemented, with low plasticity clay and silt.	1 1	55	45	26	
	1	4~		SP- SM	dense	SAND, light brown, fine to medium, poorly graded, calcareous, dry, stratified, gravel increases with depth from a trace at 3' to a little at 6', non-cemented, trace of non plastic silt.	10	82	8		
		6 ~	(((((()	CL	Stiff	SILTY CLAY, gray, low plasticity, calcareous, dry, homogeneous, nen cemented.					
	- 3	10-		SM	Medium dense	SILTY SAND. light brown, fine, quorly graded, cal-		66	33		
, !		!				Total Depth 12.5' (3.8m)		1 1			
		14-				Stability of Vertical Walls: Stable					
	-5	16 -									
		18 -									
	-6	20 -									
		22		'							

TRENCH DETAILS

SURFACE ELEVATION : 3320' (1012m)
DATE EXCAVATED : 11 December 1977

SURFACE GEOLOGIC UNIT : A40

TRENCH LENGTH : 28" (8.5m)

TRENCH ORIENTATION : N75W

LOG OF TRENCH SS-T-5 SAN SIMON VALLEY, ARIZONA HIGHLANDS CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

C-6

	_	1		Ĭ				-	PERCE	NT FIN	ER BY	WEIGHT				
ب و و	E R (a)	SAMPLE I	NTERVAL		S	TANDAR	SIEV					S STAI		IEVE I	10	PAR
BOR ING Number	SAMPLE NUMBER	İ		BLDRS.	COB	BLES		GRA	VEL			12	ND		SII	T OR
	SAI	FEET	METERS	24"	12"	6"	3"	1岁"	3 4"	3 8"	4	10	40	100	200	.005
35-B-1	77-1	0-2.5	0.61-0.76	Î								†				
	D - 2	10.0-10.5	3.05-3.20	1 1				100	84	69	50	36.	23	1.3	7	
	1	10.0-10.5	3.05-3.20	†					1	1	†	† ····	† 		† ·	İ
		10.0-11.5	3.05-3.20	1							Ì	1	† ·		† · · · -	İ
	D−3	15.0-15.3	4.57-4.63	1			Ī · · ·				İ	†	† - · · -		†	†
	P=4	21.4-32.2	0.52-6.77	1			Ī -					100	49	98	95	27
	Γ-	25.4-25.7	7.62-7.83	1						1	†	†	† 	†		† ¨
	₽-e	30.0-30.7	9.14-9.36			<u> </u>				T		1	† -		†	
		30.7-31.4	9.36-9.57	1		T			1			1	100	99	914	- 6 , t
	t	61.4-32.4	9.57-9.88						<u> </u>	1		† 	+	 	t	† —
	11-7	40.7-41.4	12.41-12.64	†		l				†	t	 	 	†	†	 -
		50.7-51.4	15.45-15.67	†			\vdash		1	 	<u> </u>	 	 	 	 	 -
	F 7	00.7-61.4	18.50-18.71	t	→ •	† · · · · · · · · ·						 	 	†	† <i>-</i>	<u> </u>
	4-15	71.4-72.	/1.76-21.94	† †		†	<u> </u>		<u> </u>	1		100	10	1915	97	1
	r-11		24.60-24.87	1		·		t- -		†	†	†	 	├	t	-
	F-12		27.64-27.86		-	<u> </u>			<u> </u>	 	 	 	 	 	t	1
	F-13	100.7-101.4		 		<u> </u>	<u> </u>	· ··· -	† -	† • • • • • • • • • • • • • • • • • • •	 	+	 	t · · · · ·	t ·	t
	F-14	125.0-125.7		1		 	<u> </u>		 	 	 	 	100		99	
	<u> </u>	125.9-176.4		†		r	h		 -	<u> </u>	 	+	 	 	 	† ′
		120.4-127.0		t		<u> </u>		<u> </u>	 	 	 	+	 -	 	 	t
	P-15	153.9-150.7		t		-			 	 	 	 	 -	 	 	
	P-1c	175.7-176.4	.	1	}	†	ł	ł	t	t	†	†	 	 	t	t
	P-17	260.0-260.7	60.96-61.17	\vdash		 			 	+		 	 	 	 	 -
	P-18	225.7-226.4		 	<u> </u>	\vdash	 	 	 	 	 -	100	ļ.,	 	 	
	P-19	250.7-251.4		 				 	-	+	 	1.1.00	+	90	94	₩,
	P=30		76.41-76.63 84.03-84.25	├		 	-	 	-	 		 	 	├	 	
	P-20			}		 		<u> </u>	-	 	 	 	1.36	O.C.	99	
	1,-31	300.7-301.4	91.65-91.87	╂		 			 -	 	 	+-	190	99	 '''	¹5t.
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NOTES:

(a) Sample types

(c) USCS - Unified Soil Classification System

SS - Standard split spoon

P - Pitcher

(d) * Indicates that test has been performed and results are included in this report.

D - Fugro Drive

B - Bulk

(b) NP - Not Plastic

					<u> </u>		U C 1 711				A41 D 4 D D				,				
TOLE	AT	TERBE	ec.		ļ		N-SITU			C	OMPACTE		11	(g)	. š		8		
(MM)		IITS		USCS (c)	DRY (MOISTURE Content (%)	SATURATION (%)	VOID RATIO	MAXI Dry de	MUM NSITY	OPTIMUM Moisture (%)	SPECIFIC GRAVITY OF SOLIDS	TRIAXIAL (d)	UNCONFINED COMPRESSION	DIRECT SHEAR	CONSOLIDATION	CHEMICAL	RELATIVE DENSITY
.001	L	PL	PI		(pcf)	(kg/m³)	₽ 5°	SAT	25	(pcf)	(kg. m ³)	00 W	SPE GR	₹	38	SE	SE	CHE	
			<u> </u>	SM	(#31)	(* 8/ ** /			┿	(30.7)	("" ")	 i					-		
			NE	GW-GM	110.3	1767	2.4	14.3	0.53						 -		+		
	-			;W- ,M		* / · / / -		17.1	0.33							*			
				GW-GM		·	† · · ·		 				├ -		 i	-			
1				SC	110.3	1767	15.6	79.8	0,53										 -
1.	51	29	22	CH-MH	97.5	1562	18.9	70.2	0.73						*		*	*	
				SM	104.1	1668	14.8	64.7							†				_
				CT										*					†
51	43	22	21	$\mathbb{C}\Gamma$	87.7	1405	34.0	99.7	6,92				2.68	*					
				CL				·						*					
				CL	83.3	1334	31.1	41.9	1.0										
				ür	87.3	1 398	34.0		0.93										
	;;	4		CH	81.2	1301	39.2	96.5	1.1										
	77	29	4 -	<u>CH</u>			42.7								<u> </u>				↓
- 4				СН	87.7	1405	39.)	100	0.92						 _				ļ
. 1	· ·			<u>_CH</u> _ ⊣	82.6	1323	46.1	100	1.0						-			<u> </u>	
- ; , -	72			CH	30.4	1288	39.8	3 8.0	1.1										
-		(41.	CH CH			45.3					 		*		-	-		├
	• •	·		CH			45.1							*	*				┼
				CH	96.5	1543	211 2	7 1/1							 	 			+-
į	İ	1		MI.	99.4	$\frac{1343}{1592}$	38.2 36.3		0.75			<u> </u>			 				1 -
_				CH CH	102.	1655	31.8	100	0.70						+			L	
		25	41	CH		1455	32.7	100	$\frac{0.63}{0.86}$				 		+ *	1	 -		<u> </u>
				СН	117.9	1710	23.3	100	0.56		L				†	 			1
				CH	88.9	1424	33.3	100	U. 89				1	<u> </u>	 				
11.	55	22	33	CH	92.6	1483	31.8	100	0.82			·							
								1000	0.02										
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SUMMARY OF LABORATORY TEST RESULTS

BORING SS-B-I
SAN SIMON VALLEY, ARIZONA, HIGHLANDS CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SAMSO

C-1

													_						 		
HEIGHT	OIAMETER	2.4	2.4	2.4	2.4	2.4	2.4	2.4	2.4	2.4											
DEGREE OF	(%)	81.0	100	100	48.6	49.4	69.2	45.3	35.7	78.8											
MOISTURE	(%)	25.9	31.8	30.4	10.2	10.0	13.3	13.5	10.1	12.7											
	kg/m3	1447	1459	1495	1721	1746	1775	1496	1528	1519											
ORY DENSITY	pct	90.3	91.1	93.3	107.4	109.0	110.8	93.4	95.4	94.8							İ				
FINED	kN/m²	172	541	546	344	658	263	464	311	1647			•						•		
UNCONFINED COMP. STRENGTH	ksi	3.6	11.3	11.4	7.2	13.7	5.5	9.7	6.5	34.4											
-	TYPE	CH-MH	ಕ	СН	SC	כר	CL	10	CL-ML	НЭ											
NTERVAL	METERS	6.58-6.77	68.76-69.10	91.71-91.87	3.05-3.20	0.76-0.91	14.33-14.48	3.32-3.47	9.14-9.30	18.29-18.44											
SAMPLE INTERVAL	FEET	21.6-22.2	225.9-226.4	300.9-301.4	10.0-10.5	2.5-3.0	47.0-47.5	10.9-11.4	30.0-30.5	60.6-60.5											
SAMPLE	NO.	₽~d	P-18	P-21	0-3	<u>-</u>	6-0	F-3	7-0	0-10											
9	NO.	SS-B-1			SS-B-6	SS-B-7	SS-B-9	SS-B-11	SS-B-12												-

SUMMARY OF UNCONFINED COMPRESSION TEST RESULTS

SAN SIMON VALLEY, ARIZONA, HIGHLANDS CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

TABLE C-2

BACK PRESSURE	kN/m^2	0	0	0	0								
PRES	ksi	0	0	0	-								
STRAIN	(% min)	0.1	0.1	0.1	0.1								
MUM VI - Oz	kN/m ²	680	1283	1087	2361								
MAX DEVI	ksi	14.2	26.8	22.7	49.3								
KING F(O ₃)	kN/m ²	158	632	484	484			i					
CONFINING PRESSURE (03) S	ksf	3.3	13.2	10.1	10.1								
MOISTURE CONTENT	(%)	28.7	27.4	9.4	8.0								
1 1	kg/m³	1496	1517	1852	2025								
DRY DENSITY	pc f	93.4	94.7	115.6	126.4								
TYPE 0F	rest	93	8	8	3								
_	TYPE	13	2	13-38	73-3S								
INTERVAL	METERS	9.34-9.57	9.72-9.88	15.30-15.45	15.58-15.73								
SAMPLE	FEET	30.7-31.4	31.9-32.4	50.2-50.7	51.1-51.6								
SAMPLE	2	P-6	P-6	P-9	P-9								
2	9	SS-B-1		SS-B-11									

SUMMARY OF TRIAXIAL SHEAR TEST RESULTS
SAN SIMON VALLEY, ARIZONA
HIGHLANDS CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

C-3

BORING	SAMPLE	SAMPLE 1	NTERVAL	SOIL	NORMAL	STRESS	MAXI SHEAR S	MUM STRENGTH
NO.	NO.	FEET	METERS	TYPE	ksf	kN/m²	ksf	kN/m ²
SS-B-1	D - 2	10.0-10.5	3.05-3.20	GW-GM	1.0	48	1.3	62
	D-2	10.0-10.5	3.05-3.20	GW-GM	2.0	96	1.6	77
	D-2	10.0-10.5	3.05-3.20	GW-GM	4.0	192	2.8	134
SS-B-2	0-1	2.0-2.5	0.61-0.76	CH	0.2	10	1.6	17
	D-1	2.0-2.5	0.61-0.76	CH	0.5	24	2.0	96
	D-1	2.0-2.5	0.61-0.76	CH	1.0	48	4.8	230
	P-3	10.9-11.4	3.32-3.47	SC	1.0	48.	1.7	81
-	P-3	10.9-11.4	3.32-3.47	SC	2.0	96	3.4	163
	P-3	10.9-11.4	3.32-3.47	SC	4.0	192	5.7	273
SS-B-3	D-3	10.0-10.5	3.05-3.20	SM	1.0	48	0.8	38
	D-3	10.0-10.5	3.05-3.20	SM	2.0	96	1.5,	72
	D-3	10.0-10.5	3.05-3.20	SM	4.0	192	3.7	177
SS-B-4	D-1	2.5-3.0	0.76-0.91	SM	0.2	10	0.4	19
	0-1	2.5-3.0	0.76-0.91	SM	0.5	24	0.5	24
	D-1	2.5-3.0	0.76-0.91	SM	1.0	48	0.8	38
SS-B-6	D-1	2.5-3.0	0.76-0.91	CL	0.2	10	0.6	29
	D-1	2.5-3.0	0.76-0.91	CL	0.5	24	0.9	43
	0-1	2.5-3.0	0.76-0.91	CL	1.0	48	3.7	177
SS-B-11	D-1	2.0-2.5	0.61-0.76	SM	0.2	10	0.5	24
	D-1	2.0-2.5	0.61-0.76	SM	0.5	24	0.5	24
	0-1	2.0-2.5	0.61-0.76	SM	1.0	48	2.0	96
SS-8-13	D-2	5.0-5.5	1.52-1.68	SC	0.5	24	1.5	72
	D-2	5.0-5.5	1.52-1.68	SC	1.0	48	2.0	96
	D-2	5.0-5.5	1.52-1.68	32	2.0	96	4.3	206

SUMMARY OF DIRECT SHEAR TEST RESULTS SAN SIMON VALLEY, ARIZONA HIGHLANDS CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

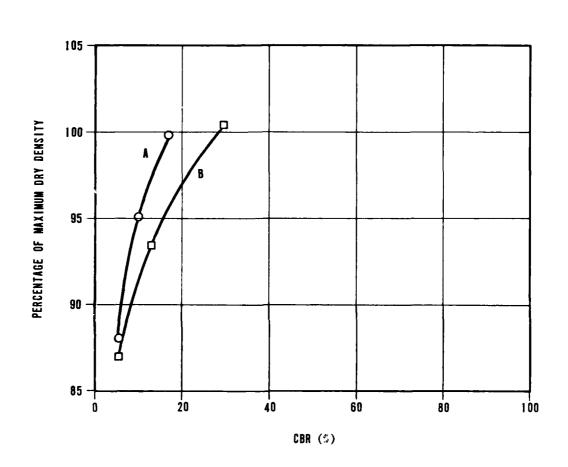
C-4

CBR	(%)	9	01	11		9	El	30							
PERCENT OF MAXIMUM	DRY DENSITY	88.1	95.1	83.8		87.0	93.5	100.7							
COMPACTED	(%)	10.5	10.2	10.6		12.2	12.1	12.0							
COMPACTED DRY DENSITY	kg/m3	1775	1916	2011		1703	1831	1972							
P .	pcf	110.8	119.8	125.5		106.3	114.3	123.1							
OPT INUM MOISTURE	(%)			10.5				12			-				
MAXIMUM DRY DENSITY	kg/m³			2015				1958							
MAX DRY DE	pc f			125.8				122.2	 					 	
SPECIFIC	GKAVIIT														
ATTERBERG LIMITS	PI							_							
ATTE	11							26							
PERCENT PASS ING	#200			æ				45							
1108				၁၄				- SC-SH							
COMPOSITE	NUMBER			~											

CALIFORNIA BEARING RATIO (CBR) TEST RESULTS SAN SIMON VALLEY, ARIZONA, HIGHLANDS CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

C-5



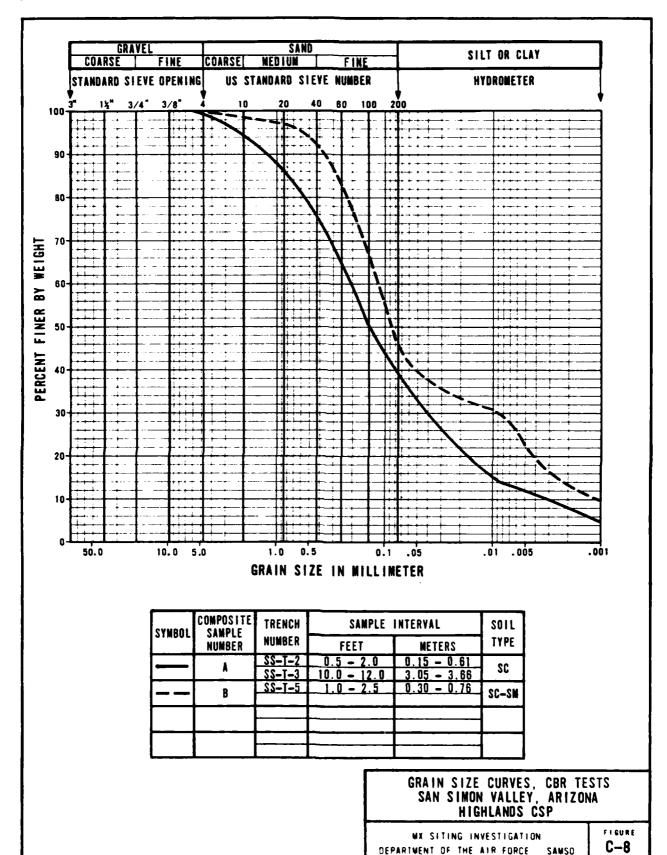
SYMBOL	COMPOSITE Sample Number	SOIL TYPE
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	В	SC-SM

CALIFORNIA BEARING RATIO (CBR) CURVES SAN SIMON VALLEY, ARIZONA, HIGHLANDS CSP

MX SITING INVESTIGATION

DEPARTMENT OF THE AIR FORCE SANSO

C-7



DATE FILMED 4-82

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